

PATENT ABSTRACTS OF JAPAN

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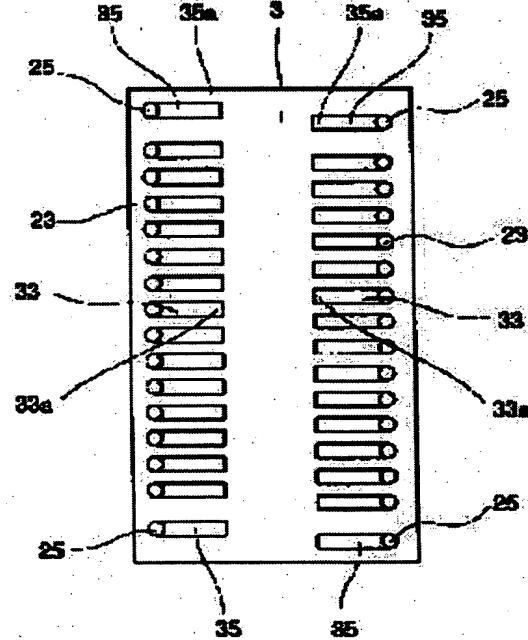
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(54) INK JET RECORDER

(57)Abstract:

PROBLEM TO BE SOLVED: To enhance reliability while reducing the size and cost by providing a pattern connecting with a printed board in a region other than a region where means for connecting a pressure generating means with a plane other than that provided with the pressure generating means is formed.

SOLUTION: Discrete end face terminal on the side of end face not facing each piezoelectric element in each array of piezoelectric elements is connected with discrete lead-out electrode on a substrate 3 through a conduction processing material. Each discrete lead-out electrode and a common electrode are conducted with a connection pattern, i.e., a rear surface discrete electrode pattern 33 and a rear surface common electrode pattern 35, through through-hole electrodes 23, 25, respectively. A printed board, i.e., an FPC, is connected at a connection region (connecting part, contact part) with a flexible print cable FPC and applied with a drive voltage. Consequently, a field is generated in the laminating direction and an elongation is induced in the piezoelectric element in the laminating direction.



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CLAIMS

[Claim(s)]

[Claim 1] A nozzle which carries out the regurgitation of the ink drop A liquid room which this nozzle opens for free passage A pressure generating means to generate a pressure to which this liquid indoor capacity is changed A printed circuit board in which a pattern for carrying an ink jet arm head which formed this pressure generating means in a substrate, and impressing an actuation wave to said pressure generating means of this ink jet arm head was formed It is the ink jet recording device equipped with the above, and is characterized by having established a connecting means which connects to said substrate fields and said pressure generating means other than a field in which said pressure generating means was formed, and preparing a connection pattern connected with said printed circuit board in fields other than a field which formed this connecting means further.

[Claim 2] It is the ink jet recording device characterized by having connected to a publication fields and said pressure generating means other than a field which established said pressure generating means through a breakthrough which formed said connecting means in said substrate in an ink jet recording device at claim 1, and preparing said connection pattern in a rear face of said substrate.

[Claim 3] An ink jet recording device characterized by covering a part of field [at least] except a field which connects a pattern of said printed circuit board with a material which has insulation in an ink jet recording device according to claim 1 or 2.

[Claim 4] An ink jet recording device characterized by the maximum array pitch of said connection pattern being more than an array pitch of said connecting means in an ink jet recording device according to claim 1 to 3.

[Claim 5] An ink jet recording device characterized by carrying out two or more trains arrangement of said connecting means in an ink jet recording device according to claim 1 to 4.

[Claim 6] An ink jet recording device characterized by carrying out two or more trains arrangement of the inlet connection with said printed circuit board of said connection pattern in an ink jet recording device according to claim 1 to 5.

[Claim 7] An ink jet recording device characterized by for an ink jet recording device according to claim 1 having set, having arranged two or more trains of said pressure generating means, having established a connecting means of two or more trains corresponding to each, and preparing inlet connection with said printed circuit board inside said connecting means.

[Claim 8] An ink jet recording device characterized by stationing inlet connection with a printed circuit board of said connection pattern at both sides of said connecting means in an ink jet recording device according to claim 1 to 7.

[Claim 9] An ink jet recording device characterized by connecting said connection pattern and printed circuit board with a different direction electrical conducting material in an ink jet recording device according to claim 1 to 8.

[Claim 10] An ink jet recording device characterized by carrying two or more ink jet arm heads, and preparing at least two or more of ink jet arm heads of it on one printed circuit board in an ink jet recording device according to claim 1 to 9.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Industrial Application] Especially this invention relates to the connection structure of an ink jet arm head and a printed circuit board about an ink jet recording device.

[0002]

[Description of the Prior Art] An ink jet recording device does not almost have the oscillation at the time of record, and the noise, and since especially colorization is easy, it is used for others, facsimile, a copy machine, etc. which output the data of digital processors, such as a computer. [printer] The ink jet arm head used for such an ink jet recording device drives actuator means (pressure generating means), such as a piezoelectric device (piezo mold), an exoergic resistor (bubble mold), a diaphragm, and a counterelectrode (electrostatic type), according to a record signal, carries out regurgitation flight of the ink drop from a nozzle, and performs image recording on a record medium.

[0003] for example, as an ink jet arm head using a piezoelectric device While joining to two or more trains seriate and arranging two or more laminating mold piezoelectric devices on a head substrate as indicated by JP,8-142324,A etc. The frame member located in the perimeter of a piezoelectric device is joined. On these piezoelectric devices and a frame member Carry out the laminating of the diaphragm which has the diaphragm section, and the laminating of the liquid room septum member which forms the ink supply way which supplies ink to the application-of-pressure liquid room pressurized through the diaphragm section by the laminating mold piezoelectric device on this diaphragm and this liquid room is carried out. Furthermore, the laminating of the nozzle plate in which the nozzle was formed on this liquid room septum member is carried out, and there is a thing it was made to make an ink drop breathe out from a nozzle with the variation rate of the d33 direction of a laminating mold piezoelectric device.

[0004] It is necessary to connect electrically between the printed circuit boards which mounted the driver (actuation IC) for impressing a necessary actuation wave to a piezoelectric device and a piezoelectric device, and the wirebonding method is conventionally used in the ink jet arm head using such a piezoelectric device (JP,6-320721,A).

[0005] However, in the case of the wirebonding method, it is necessary to choose that gold plate must be used for the electrode material of a head end substrate and a printed circuit board lateral electrode etc. Moreover, in order to make 1 sequential 1 connection, the number of wirebonding also increases, in the case of a high accumulation nozzle (for example, 100 or more nozzles), working hours are long, and cost also becomes high. Furthermore, as for the wirebonding section, it has many problems that there is the need of closing in order to protect from the open circuit by contact of wires, mixing of an impact and a foreign matter, etc.

[0006] Then, there is the method of connecting the electrode and flexible printed cable (FPC) of a piezoelectric device on a direct pewter and different direction electric conduction tape as indicated by JP,6-320721,A.

[0007] Moreover, as a connection method of a flexible patchboard, the tabular piezo electric crystal which arranged the electrode on the surroundings is inserted with a bottom substrate and a top substrate,

two or more through hole electrodes are drilled on the outskirts of each of one substrate and a tabular piezo electric crystal, and the method of connecting an actuation electrode and a flexible substrate through a through hole is learned as indicated by JP,5-28673,U.

[0008]

[Problem(s) to be Solved by the Invention] However, if it is in the structure which carries out direct continuation of the piezoelectric device mentioned above and FPC, since there is inlet connection (it is also called the contact section and a surface of action.) with FPC in the same direction as the nozzle of a substrate side, thoroughgoing protection for preventing that ink adheres and inter-electrode leaks must be carried out. Moreover, since the contact section with FPC does not have a passage board, common ******, and a nozzle plate and the front face needs to be exposed, it is necessary to take out a piezoelectric device to an excess at least more than the length of the contact section, and the magnitude of a piezo electric crystal becomes large.

[0009] Moreover, if it is in the structure using a through hole Since it is connectable with a flexible substrate in respect of a piezo electric crystal and a reverse substrate, Irregularity becomes large considerably at ** which forms a through hole in the substrate of the thing it becomes unnecessary to enlarge the thoroughgoing protection and the thoroughgoing piezo electric crystal for preventing the contamination in ink etc. The sake, It is unknown a flexible substrate and for reliability to be good and to connect with the sufficient yield, as long as it is indicated by the above-mentioned official report.

[0010] This invention is made in view of the above-mentioned point, and it aims at offering the ink jet recording device which can realize densification of the ink jet arm head to carry, miniaturization, low-cost-izing, and high-reliability.

[0011]

[Means for Solving the Problem] In order to solve the above-mentioned technical problem, an ink jet recording device of claim 1 A nozzle which carries out the regurgitation of the ink drop, a liquid room which this nozzle opens for free passage, and a pressure generating means to generate a pressure to which this liquid indoor capacity is changed, In an ink jet recording device which has a printed circuit board in which a pattern for carrying an ink jet arm head which formed this pressure generating means in a substrate, and impressing an actuation wave to said pressure generating means of this ink jet arm head was formed It considered as a configuration which established a connecting means which connects to said substrate fields and said pressure generating means other than a field in which said pressure generating means was formed, and prepared a connection pattern connected with said printed circuit board in fields other than a field which formed this connecting means further. In addition, it uses for a "printed circuit board" in semantics containing a printed circuit board (PCB), flexible printed cable (FPC), and conductivity film etc.

[0012] In an ink jet recording device of above-mentioned claim 1, an ink jet recording device of claim 2 connected fields and said pressure generating means other than a field in which said pressure generating means was formed through a breakthrough formed in said substrate, and considered said connecting means as a configuration which prepared said connection pattern in a rear face of said substrate.

[0013] An ink jet recording device of claim 3 was considered as a configuration which covered a part of field [at least] except a field which connects a pattern of said printed circuit board with a material which has insulation in above-mentioned claim 1 or an ink jet recording device of 2.

[0014] An ink jet recording device of claim 4 was considered as a configuration whose maximum array pitch of said connection pattern is more than an array pitch of said connecting means in above-mentioned claim 1 thru/or one ink jet recording device of 3.

[0015] In above-mentioned claim 1 thru/or one ink jet recording device of 4, said connecting means considered an ink jet recording device of claim 5 as a configuration by which two or more trains arrangement is carried out.

[0016] In above-mentioned claim 1 thru/or one ink jet recording device of 5, inlet connection with said printed circuit board of said connection pattern considered an ink jet recording device of claim 6 as a configuration by which two or more trains arrangement is carried out.

[0017] An ink jet recording device of claim 7 was considered as a configuration which an ink jet

recording device of above-mentioned claim 1 set, has arranged two or more trains of said pressure generating means, established a connecting means of two or more trains corresponding to each, and prepared inlet connection with said printed circuit board inside said connecting means.

[0018] An ink jet recording device of claim 8 was considered as a configuration by which inlet connection with a printed circuit board of said connection pattern is stationed at both sides of said connecting means in above-mentioned claim 1 thru/or one ink jet recording device of 7.

[0019] An ink jet recording device of claim 9 considered said connection pattern and printed circuit board as a configuration connected with a different direction electrical conducting material in above-mentioned claim 1 thru/or one ink jet recording device of 8.

[0020] In above-mentioned claim 1 thru/or one ink jet recording device of 9, an ink jet recording device of claim 10 carried two or more ink jet arm heads, and at least two or more of ink jet arm heads of it considered it as a configuration prepared on one printed circuit board.

[0021]

[Embodiment of the Invention] Hereafter, the gestalt of operation of this invention is explained with reference to an accompanying drawing. Hereafter, the gestalt of operation of this invention is explained with reference to an accompanying drawing. The important section enlarged view of drawing 3 and drawing 6 of the important section expanded sectional view to which the appearance perspective diagram and drawing 2 which show an example of the ink jet head section of the ink jet recording device which drawing 1 requires for the 1st operation gestalt of this invention meet the decomposition perspective diagram of this ink jet arm head, and drawing 3 meets the A-A line of drawing 1, the important section expanded sectional view to which drawing 4 meets the B-B line of drawing 1, and drawing 5 are rear-face drawings of a substrate.

[0022] This ink jet arm head consists of an actuator unit 1 and a liquid room unit 2 joined on this actuator unit 1. The actuator unit 1 has joined the frame member 5 which encloses the perimeter of the piezoelectric-device trains 4 and 4 of two trains which come to arrange two or more laminating mold piezoelectric devices in the shape of a train on the insulating substrate 3 (successive installation), and the piezoelectric-device train 4 of these 2 train with adhesives 6. The piezoelectric-device train 4 consists of two or more piezoelectric devices 7 to which the driving pulse for drop-izing ink and making it fly is given.

[0023] The liquid room unit 2 pastes up the passage septum member 13 which consists of metal plates, such as a photopolymer film (dry film resist) which forms an application-of-pressure liquid room, common ink passage, etc. on the diaphragm 12 in which the diaphragm section 11 was formed, or SUS, with the thermocompression bonding of a dry film resist, or adhesives, and comes to paste up the nozzle plate 15 in which two or more nozzles 14 were formed on this passage septum member 13.

[0024] By these diaphragms 12, the passage septum member 13, and the nozzle plate 15 The flow-resistance section 18 which serves as an ink supply way which supplies ink to the application-of-pressure liquid room 16 from the common liquid room 17 arranged on both sides of two or more application-of-pressure liquid rooms 16 which each achieved abbreviation independence, and each application-of-pressure liquid room 16 which have the diaphragm section 11 which counters the piezoelectric device 7 of each piezoelectric-device train 4, and the common liquid room 17 is formed. And each piezoelectric device 7 was countered and the nozzle 14 which is open for free passage in the application-of-pressure liquid room 16 is arranged. And that diaphragm 12 has joined this liquid room unit 2 to the actuator unit 1 with high rigidity with adhesives.

[0025] Here, the substrate 3 of the actuator unit 1 consists of a thing of the construction material which moreover resembled the piezoelectric device by about 0.5-5mm in thickness, it is desirable for a cut according to a diamond wheel in a piezoelectric device to be possible, and it is [corresponding to a piezoelectric device 7, it is high-density, and] desirable [the substrate] that a through hole can be formed.

[0026] The individual drawer electrode 22 for giving a selection signal to each piezoelectric device 7 divided in the slit slot 21 which connects the end-face side which not each piezoelectric device 7 of each piezoelectric-device train 4 counters was formed in the both ends of the successive installation direction

of the piezoelectric device 7 of this substrate 3, and the direction which goes direct, and each individual drawer electrode 22 is connected to the rear-face side of a substrate 3 through the through hole electrode 23 which is a connecting means. Moreover, between each piezoelectric-device train 4 and 4, the common electrode 24 for giving an actuation wave to each piezoelectric device was formed, and the common electrode 24 is connected to the rear-face side of a substrate 3 through the through hole electrode 25 which is a connecting means.

[0027] Here, the physical relationship with a piezoelectric device 7, the individual drawer electrode 22, and the common electrode 24 is leaving the crevice slightly, as shown in drawing 5. This is because the thickness and the error of electrodes 22 and 24 will affect the cementation quality of a piezoelectric device 7, i.e., the field parallel precision after the homogeneity of cementation, or cementation, and are not desirable, if a piezoelectric device 7 appears on each electrode 22 and 24. However, if a piezoelectric device 7, the individual drawer electrode 22, and the common electrode 24 are the degrees which overlap slightly, there are few adverse effects.

[0028] Moreover, a piezoelectric device 4 consists of a laminating mold piezoelectric device of ten or more layers, as shown in drawing 3 and drawing 5, and it carries out the laminating of the thickness of 20-50 micrometers / PZT (=Pb(Zr-Ti)O₃)₂₆ of one layer, and the internal electrode 27 that consists of thickness of several micrometers / the silver and PARAJUMU of one layer (AgPd) by turns. And it is considering as the inactive layer without forming the electrode equivalent to an internal electrode 26 in the upper surface of maximum upper 26a of a piezoelectric device 7. In addition, the material used as a piezoelectric device is not restricted above, and can also use the ferroelectric of BaTiO₃, PbTiO₃, and NbO(NaK)₃ grade generally used as a piezoelectric-device material.

[0029] And many internal electrodes 27 of the piezoelectric device 7 of each piezoelectric-device train 4 are taken out to an ends side by turns every other layer. It connects with the individual end-face electrodes 28 and 29 which were formed in the ends side and which consist of AgPd, for example. The individual end-face electrode 28 by the side of the end face which each piezoelectric device 7 of each piezoelectric-device train 4 counters is connected to the common electrode 24 on a substrate 3 through the with a 200 kgf/mm Young's modulus [or more 2] flow processing material 30. The individual end-face electrode 29 by the side of the end face which each piezoelectric device 7 of each piezoelectric-device train 4 does not counter is connected to the individual drawer electrode 22 on a substrate 3 through the flow processing material 31.

[0030] The rear-face individual electrode pattern 33 and the rear-face common electrode pattern 35 which are a connection pattern are made to flow through the through hole electrodes 23 and 25, respectively, as the drawer electrode 22 classified by each and the common electrode 24 are shown in drawing 6. In a connection field (inlet connection, contact section) with each FPC37, FPC37 which is a printed circuit board is connected (refer to drawing 1), and electric field occur in the direction of a laminating by the ability giving driver voltage. In a piezoelectric device 7, the variation rate (variation rate of d33 direction of electric field and this direction) of the elongation of the direction of a laminating occurs.

[0031] The frame member 5 is plate-like part material which a green expansion coefficient becomes from the thermosetting molding material of the epoxy resin system not more than 2x10⁻⁶/degree C, and drills the bore sections 38 and 39 corresponding to the piezoelectric-device train 4. It is a fixed part to the one side of the successive installation direction of each piezoelectric device 7, and the direction which intersects perpendicularly. While forming 40 and 41, a fixed part 42 is formed also in the center section which is the other side of two piezoelectric-device trains 4, and the bridge formation section 43 is formed in the both ends of the successive installation direction of each piezoelectric device 7 of these fixed parts 40-42. In addition, ink feed-holes 5a corresponding to ink feed-holes 3a of a substrate 3 is formed in one bridge formation section 43 of the frame member 5.

[0032] And as shown in drawing 3, the conductive paste (conductive cement) 44 is applied to the whole surface, the common electrode 24 divided into every each piezoelectric-device 7 (each channel) in the slit slot 21 is connected mutually, and the common electrode 24 of one is formed in fixed part 42 underside of this frame member 5.

[0033] Next, as shown in drawing 3, the application-of-pressure liquid room 16 side makes a flat side the diaphragm 12 of the liquid room unit 2, it forms diaphragm field 12a from which thickness differs, and cementation field 12b, and the piezoelectric-device train 4 side forms the diaphragm section 11 corresponding to the piezoelectric device 7 of the piezoelectric-device train 4, respectively. This diaphragm 12 consists of a metal plate of nickel (nickel), and is manufactured by the electroforming method. In addition, 12d of ink feed holes is formed also in a diaphragm 12.

[0034] The passage septum member 13 is located between the diaphragm 12 upper surface and a nozzle plate 15, forms the passage of the application-of-pressure liquid room 16 etc., and constitutes it from the manufacturing process by the bottom passage septum member 51 and the upside passage septum member 52.

[0035] The bottom passage septum member 51 consists of the photopolymer film or SUS substrate adhered to the diaphragm 12 upper surface. As shown in drawing 3, while forming the passage of the application-of-pressure liquid room 16 grade which became independent respectively corresponding to the upside passage septum member 52 and each piezoelectric device 7 of the *** intermediary piezoelectric-device train 4. It consists of the inside septum section 53 of a large number which form the flow-resistance section 18 which served as the ink supply way to each application-of-pressure liquid room 16, and the periphery septum section 54 which forms the common liquid room 17 in the perimeter of the application-of-pressure liquid room 16. Although the upside passage septum member 52 is the same configuration as the bottom passage septum member 51 and abbreviation, they differ at a point without the portion equivalent to the flow-resistance section 18 of the bottom passage septum member 51.

[0036] The nozzle 14 of a large number which are the micropores for making an ink drop fly is formed in the nozzle plate 15, and the path of this nozzle 14 was formed in 50 micrometers or less for the diameter of an ink drop outlet side, and the nozzle 14 is formed in the location [/ near the center of the application-of-pressure liquid room 16]. This nozzle plate 15 as well as a diaphragm 12 consists of a metal plate of nickel, and is manufactured by the electroforming method.

[0037] In addition, although this operation gestalt showed the example which establishes the common liquid room 17 in the both sides of the application-of-pressure liquid room 16, and performs ink supply from both sides, the configuration which prepares a common liquid room and the flow-resistance section only in one side, and carries out ink supply from one side may be used. Moreover, especially the location of a nozzle is not what was restricted in the center, and may be prepared near the edge of an application-of-pressure liquid room.

[0038] Next, the manufacturing process of this ink jet arm head is explained. This ink jet arm head is joining with glue and manufacturing both the units 1 and 2, after attaching independently the actuator unit 1 and the liquid room unit 2 beforehand. Since the actuator unit 1 which dust etc. tends to generate at a processing assembly process, and the liquid room unit 2 which wants to avoid adhesion of dust etc. thoroughly can be attached at a separate process while the excellent articles of both the units 1 and 2 can be chosen and attached and the yield improves by adopting such a manufacturing process, the quality of the completed ink jet arm head itself improves.

[0039] Hereafter, it explains concretely. First, processing of the actuator unit 1 and the assembly process are as follows. That is, as shown in drawing 7, ink feed-holes 3a is beforehand formed in the substrate 3 formed from electric insulation materials, such as ceramics and resin of high rigidity. Furthermore, through holes 23a and 25a are formed in a part of location which forms the location and common electrode used as an individual drawer electrode.

[0040] And while forming the pattern 61 for individual drawer electrodes which becomes the both-sides portion of this substrate 3 from the conductive material for forming the individual drawer electrode 22, the pattern 62 for common electrodes which consists of a conductive material is formed so that substrate 3 center and the pattern 61 for individual drawer electrodes may be bypassed and the both ends of a substrate 3 may be attended, and let between the pattern 61 for individual drawer electrodes, and the patterns 62 for common electrodes be the piezoelectric-device cementation field 63. Furthermore, after forming them, simultaneously with formation of the pattern 61 for individual drawer electrodes, and the

pattern 62 for common electrodes, the layer which also becomes through hole 23a and an interior wall of 25a from a conductive material may be formed.

[0041] Moreover, as shown in drawing 6, the rear-face individual electrode pattern 33 is formed from the through hole electrode 23 of the individual drawer electrode 22 to inlet connection with FPC37, and the rear-face common electrode pattern 35 is formed in the rear face of this substrate 3 from the through hole electrode 25 of the common electrode 25 to inlet connection with FPC37. Then, through holes 23a and 25a are filled up with the good material of energization nature, such as Ag, and the through hole electrodes 23 and 25 are formed. The restoration method makes Ag the shape of a paste, and it is poured into the interior of through hole 23a and 25a, and it can perform it easily by making it dry and solidify.

[0042] Furthermore, it is desirable that pattern formation covers the portion except inlet connection with FPC37 of the rear-face individual electrode pattern 33 of the rear face of a substrate 3 and the rear-face common electrode pattern 35 with the insulation of a photopolymer etc. with an easy material at least. This is for performing FPC mounting which prevents that inter-electrode contacts by the flash of solder, or spilling, and has reliability more at the time of connection of FPC37.

[0043] For example, as a coat pattern by the photopolymer 69, as are shown in drawing 8, and it is good and is indicated except the portion except the connection fields 33a and 35a with FPC37 in drawing 9 as *****, portions other than connection field 33a with FPC of each train and 35a may be covered, or between FPC connection field 33a which adjoins as shown in drawing 10, and 35a may be covered.

[0044] Moreover, the FPC connection fields 33a and 35a of the rear-face individual drawer electrode pattern 33 which is a connection pattern, and the rear-face common electrode pattern 35 are formed inside a substrate 3 from the location of through holes 23a and 25a, as shown in drawing 6. Thereby, in order to form inlet connection with FPC37, a substrate 3 does not become large and the miniaturization of an arm head can be attained.

[0045] Each of these electrodes (electrode pattern) 22, 24, 33, and 35 are formed by methods, such as printing of thick-film-conductor pastes, such as metal vacuum evaporationo of nickel, Au, Cu, etc. or electrolysis of a metal of the same kind, non-electric-field plating or AgPd, AgPt, and Au paste, and are stuck to the 3rd page of a substrate.

[0046] And the piezoelectric-device plate 64 which forms a laminating mold piezoelectric device in said piezoelectric-device cementation field 63 on a substrate 3 in the shape of a plate (the shape of or a sheet), and becomes as shown in drawing 11 is joined with glue using adhesives (refer to drawing 3). As adhesives used for cementation to the substrate 3 of this piezoelectric-device plate 64, a with a 200 kgf/mm Young's modulus [or more 2] thing is good, and is using the epoxy system adhesives of a heat hardening mold here. As a gestalt of adhesives, film 1 liquid type, 2 liquid mixing type, or a type etc. is usable.

[0047] And the end-face electrode for forming the individual end-face electrodes (individual external electrode) 28 and 29 in the short side part end face of these piezoelectric-device plates 64 beforehand is formed. While connecting electrically to the pattern 62 for common electrodes on a substrate 3 the near end-face electrode with which these two piezoelectric-device plates 64 counter after joining with glue to a substrate 3 top with the flow processing material 30 The end-face electrode with which two piezoelectric-device plates 64 do not counter is electrically connected to the pattern 61 for the drawer electrodes classified by each on a substrate 3 with the flow processing material 31. As these flow processing materials 30 and 31, the with a 200 kgf/mm Young's modulus [or more 2] thing is used. Moreover, as a flow processing material, dipping, such as vacuum evaporationo of sputtering, such as electroconductive glue and Au, Au, etc. and AgPd, etc. can be used, for example.

[0048] Subsequently, slit processing which cuts the surface section of two piezoelectric-device plates 64 and substrates 3 by the dicer which set the diamond wheel in the pitch by which the piezoelectric device 7 with a width of face of about 100 micrometers [per predetermined pitch, for example, one pitch,] is formed in the direction which intersects perpendicularly with the end-face electrode is performed, and it divides into the individual end-face electrodes 28 and 29 simultaneously corresponding to each piezoelectric device 7 for an end-face electrode which carry out division formation of two or more laminating mold piezoelectric devices 7.

[0049] While making each piezoelectric device 7 become independent thoroughly by cutting deeply to the predetermined depth to a substrate 3, and putting in and cutting the slit slot 21 at this time as shown also in drawing 5, the pattern 61 for individual drawer electrodes is individually divided into the individual drawer electrode 22 corresponding to each piezoelectric device 7, respectively. In this case, the pattern 62 for common electrodes on a substrate 3 will also be divided corresponding to the piezoelectric device 7 of each [part / that].

[0050] In addition, the individual drawer electrode 22 by which division formation was carried out is connected through the individual end-face electrode 29 and the electric conduction processing material 31 by the side of the end face which not each piezoelectric device 7 counters. Moreover, the pattern 62 for common electrodes is also connected through the individual end-face electrode 28 and the electric conduction processing material 30 by the side of the end face which the piezoelectric device 7 of each piezoelectric-device train 4 counters.

[0051] Thus, while forming the pattern 61 for drawer electrodes on the insulating substrate 3. The laminating mold piezoelectric device 64 which made flow connection is joined to the end-face electrode which took out the internal electrode 27 to the ends side by turns beforehand, and was formed in each end face. After carrying out flow processing of the pattern 61 for drawer electrodes, and the end-face electrode of the laminating mold piezoelectric device 64 and connecting, while performing slit processing to the surface section of the laminating mold piezoelectric device 64 and a substrate 3 simultaneously and forming two or more piezoelectric devices 7. By dividing the pattern 61 for drawer electrodes, and an end-face electrode into two or more individual drawer electrodes 28 and individual end-face electrodes 29 respectively and individually corresponding to a piezoelectric device 7. When high density integration of two or more piezoelectric devices can be attained and drawing of the electrode from an internal electrode 27 becomes easy, since a substrate is joined to a piezoelectric device and bonding strength is high, failure of the piezoelectric device at the time of slit processing can decrease, the yield can improve, and the cutback of cost can be aimed at.

[0052] And by using a with a 200 kgf/mm Young's modulus [or more 2] thing as flow processing materials 30 and 31 which make it flow through the end-face electrode of a laminating mold piezoelectric device, and the drawer electrode on a substrate, an oscillation with a piezoelectric device and a substrate can be reduced and failure of the laminating mold piezoelectric device at the time of slit processing decreases further. Moreover, while being able to reduce an oscillation with a laminating mold piezoelectric device and a substrate and being able to lessen failure of the piezoelectric device at the time of slit processing by using a with a 200 kgf/mm Young's modulus [or more 2] thing as adhesives of a substrate 3 and a piezoelectric device 7, decline in the displacement effectiveness at the time of actuation of a piezoelectric device 7 is prevented, and the property of an arm head can be improved.

[0053] Thus, the frame member 5 is joined with glue using the adhesives which consist of with a 200 kgf/mm Young's modulus [or more 2] heat hardening mold epoxy system adhesives on the substrate 3 which slit processing of piezoelectric-device plate 64 grade ended. At this time, by applying the conductive paste 44 to the rear face of the fixed part 42 of this frame member 5, the pattern 62 for common electrode formation divided by slit processing is connected mutually, and the common electrode 24 is formed.

[0054] Here, as for the frame member 5 upper surface after joining the frame member 5, and the piezoelectric-device 7 upper surface, precision needs to serve as the same flat surface good. This is because the diaphragm section 11 which will not be pasted up if profile irregularity is bad occurs in order to join the diaphragm 12 of the liquid room unit 2 to this portion so that it may mention later.

[0055] Then, after making surface treatment possible as an inactive layer without forming an electrode in the upper surface of maximum upper 26a of a piezoelectric device 7, and joining the frame member 5 slightly higher than the height of a piezoelectric device 7 with glue, as the surface grinding process was performed, and grinding was performed until it could delete the upper surface of a piezoelectric device 7 slightly and became the same flat surface, the dimensional accuracy of both components and the difficulty of an adhesion method of construction are canceled.

[0056] And it joins with glue, carrying out caudad the diaphragm 12 side (plane of composition), and

carrying out alignment of the liquid room unit 2 which performed processing assembly separately on the actuator unit 1 which did in this way and was completed.

[0057] Then, as shown in drawing 12, electrode pattern 37a of FPC37 is joined for the part except the through hole section of the rear-face individual electrode pattern 33 of substrate 3 rear face, and the rear-face common electrode pattern 35 to heat by application of pressure as connection fields 33a and 35a. In addition, FPC37 had the pattern which can drive selectively the piezoelectric device 7 of the piezoelectric-device train 4, and has performed solder plating to the joint beforehand. In this case, more than the melting temperature of solder is required for the temperature when carrying out thermocompression bonding of FPC37, and it is usually 200 degrees C or more.

[0058] Although the through hole electrodes 23 and 25 can be made from arranging and calcinating the good material of the electrical conductivity of a metal wire etc. in the ceramics beforehand here, processing is difficult for this method, and it is difficult for it to realize a desired array with a sufficient precision.

[0059] Then, the method of punching and making with a drill etc. to a substrate 3 is used. This produces Breakthroughs (through hole) 23a and 25a with a drill to a substrate 3, and the good material of metaled electrical conductivity is formed in a breakthrough wall, or it produces them by filling it up with the material. This method can form the breakthrough of desired magnitude in a desired location, and is excellent in the point that it is moreover low cost with a comparatively sufficient precision.

[0060] However, by this method, since weld flash occurs mostly around a through hole, when the irregularity of a substrate becomes intense and carries out thermocompression bonding of the pewter in this portion, a poor contact becomes easy to produce the through hole section. So, by this invention, FPC mounting with sufficient reliability is attained by forming an electrode pattern from a through hole, avoiding a through hole, and carrying out thermocompression bonding in a comparatively flat substrate portion.

[0061] Moreover, as the electrical installation method with FPC, a rear-face individual electrode pattern, and a rear-face common electrode pattern, a different direction conductivity film can also be used in addition to solder. A rear-face individual electrode pattern and a rear-face common electrode pattern, and the electrode of FPC flow through a different direction conductivity film through a filler by having distributed the conductive particle (metal particles and carbon particle) called a filler into a thermosetting property or a thermoplastics film, and inserting and pressurizing [heat and] a different direction conductivity film between a rear-face individual electrode pattern and an individual common electrode pattern, and FPC. Also in the case of a different direction conductivity film, reliability improves by carrying out thermocompression bonding in a portion [flats / other than a through hole] similarly.

[0062] Furthermore, in the case of a different direction conductivity film, the solder connection method of polar zone is natural to a substrate 3 and FPC being fixed only with the solder of the polar zone, but since the resin of a different direction conductivity film serves as adhesives and fixes a substrate and FPC also in the portion in which the electrode is not formed, it is more desirable when obtaining bond strength. Moreover, by heating and pressurizing FPC below 150 degrees C, since thermocompression bonding is possible, generating of the stress in which the resin substrate of FPC carries out thermal-expansion - contraction and which it produces is reduced, there is no peeling of an electrode etc., and it is desirable.

[0063] Thus, after mounting FPC, finally, the ink delivery pipe 48 is inserted in ink feed-holes 3a of a substrate 3, and spreading hardening of the adhesives is carried out and it fixes.

[0064] Here, since coefficient of linear expansion forms the frame member 5 of the actuator unit 1 from the thermosetting molding material of the epoxy resin system not more than $2 \times 100-6/\text{degree C}$, when joining the diaphragm 12 and the frame member 5 of the liquid room unit 2 with glue, even if it carries out heating adhesion, deformation of a diaphragm 12 is not caused. Thus, since heating adhesion of the frame member 5 and the liquid room unit 2 can be carried out, assembly nature improves and cost is also reduced.

[0065] Moreover, as adhesives which join a substrate 3, the frame member 5 and the AKUCHUETAYU

knitting 1, the liquid room unit 2, and a piezoelectric device 7 and a substrate 3, as mentioned above, when Young's modulus uses the same epoxy system hot setting adhesive or more [200 kgf(s)/mm] by two, cost decreases.

[0066] If an operation of the ink jet arm head constituted as mentioned above is explained, next, by impressing the driving pulse voltage of 20-50V to a piezoelectric device 7 selectively according to a record signal The diaphragm section 11 to which the piezoelectric device 7 to which pulse voltage was impressed displaces, and a diaphragm 12 corresponds is made to transform in the nozzle 14 direction. The ink in the application-of-pressure liquid room 16 can be pressurized, and it can record by ink's serving as a drop from the nozzle 14 of a nozzle plate 15, and being injected by capacity (volume) change of the application-of-pressure liquid room 16.

[0067] And in connection with the regurgitation of an ink drop, the ink pressure in the application-of-pressure liquid room 16 declines, and some negative pressure occurs in the application-of-pressure liquid room 16 according to the inertia of the ink flow of this time. Since the diaphragm section 11 of a diaphragm 12 returns to the original location and the application-of-pressure liquid room 16 becomes original configuration by making impression of the voltage to a piezoelectric device 7 into an OFF state under this condition, negative pressure occurs further. At this time, it fills up with the ink containing the ink delivery pipe 48 which leads to the ink tank which is not illustrated in the application-of-pressure liquid room 16 from the flow-resistance section 28 through the common liquid room 27. Then, after the oscillation of the ink meniscus side of a nozzle 14 is declined and stabilized, pulse voltage is impressed to a piezoelectric device 7 for the ink drop regurgitation of a degree.

[0068] In addition, although the flow processing materials 30 and 31 which carry out flow processing are making the individual end-face electrodes 28 and 29 of the ends side of a piezoelectric device 7, and the common electrode 24 and the individual drawer electrode 22 adhere in the above-mentioned operation gestalt to a part of outside surface of the individual end-face electrodes 28 and 29 By making the flow processing materials 30 and 31 adhere all over the individual end-face electrodes 28 and 29, and performing flow processing The bonding strength of the piezoelectric-device plate 64 before slit processing to the piezoelectric-device plate 64 before becoming a piezoelectric device 7, and a substrate 3 can be raised by leaps and bounds, and failure of the laminating mold piezoelectric device at the time of slit processing can be reduced further.

[0069] Moreover, in the above-mentioned operation gestalt, although the example applied to the ink jet arm head of the side shooter method which carried out the direction of a opening of a nozzle on the displacement direction of a piezoelectric device and the same axle explained, it is applicable also to the ink jet arm head of the edge shooter method which carried out the direction of a opening of a nozzle in the displacement direction of a piezoelectric device, and the direction which intersects perpendicularly. Furthermore, in this operation gestalt, although FPC was used as a printed circuit board, even if it uses a rigid substrate (the so-called PCB substrate) without flexibility, there is same effect, but if it connects by the piezoelectric-device side in the case of a rigid substrate, since the thickness of a substrate is thick and the nonconformity that a substrate will become high from a nozzle side will arise, this invention becomes effective further.

[0070] Next, the 2nd operation gestalt of this invention is explained with reference to drawing 13 . In addition, this drawing is explanatory drawing by the side of a substrate rear face. When thermocompression bonding is carried out with the arm head of the 1st operation gestalt mentioned above using solder when densification of 100 or more dpi is performed for example, the flash of a pewter arises on the edge of an electrode, and a contiguity electrode may be contacted and it may flow.

[0071] That is, when the nozzle configuration density of a single tier is 100 or more dpi, since it is set to 254 micrometers and the through hole also corresponds with it, the array dense pitch of a nozzle is set to 254 micrometers the same [the array pitch of a through hole]. When the rear-face individual electrode pattern 33 is formed in this by the line / space =127micrometer / 127 micrometers, there are only 127-micrometer inter-electrode gaps, to it, that of a pewter may produce the amount of headers to about 160 micrometers with about 80 micrometers and a both-sides electrode at the maximum, therefore contiguity electrodes may contact.

[0072] Then, in this operation gestalt, the rear-face individual electrode pattern 33 gave breadth by having used through hole 23a for individual electrodes as the narrowest part, and has prepared surface-of-action 33a with FPC37 in the point.

[0073] Therefore, the pitch d1 of the rear-face individual electrode pattern in surface-of-action 33a becomes larger than the pitch d2 of through hole 23a for individual electrodes (d1> d2). Thereby, even if there is a flash of a pewter, it is lost that contiguity electrodes contact and FPC mounting with sufficient reliability is attained.

[0074] Next, the example from which the 3rd operation gestalt of this invention differs is explained with reference to drawing 14 and drawing 15. In addition, both drawings are also explanatory drawings by the side of a substrate rear face. With the arm head of the 1st operation gestalt mentioned above, at the time of through hole formation, a limit is to make the path of a through hole small, if a through hole is formed in one train when densification of 100 or more dpi is performed, a crack may enter by part for a wall, or when there are few walls between through holes, when the worst, a wall may be lost and through holes may be connected.

[0075] Then, in this operation gestalt, through hole 23a for rear-face individual electrode patterns is arranged alternately, and it is formed. By this, since through holes become possible [securing distance enough], they can secure the thickness of a wall greatly, and can prevent generating of a crack, the free passage of through holes, etc., and its reliability improves.

[0076] Here, surface-of-action 33a with FPC37 may be formed in one train as shown in drawing 14, or as shown in drawing 15, it may be alternately arranged like a through hole.

[0077] When a surface of action is formed in one train, the width of face of the heating press arm head of the application device for being able to carry out thermocompression bonding of the surface of action to FPC collectively, and heating and pressing FPC may come to be narrow, and since the temperature nonuniformity of a heating press arm head decreases, connection with high reliability with little dispersion can be made in all surfaces of action. Moreover, since press area becomes small, the welding pressure of the application device for obtaining a pressure required for thermocompression bonding may come to be small, and small [of thermocompression bonding equipment itself] and low-pricing can be attained.

[0078] On the other hand, since the length of the rear-face individual electrode pattern between a through hole and a surface of action can be arranged almost similarly when a surface of action is considered as the same alternate array as a through hole, can make wiring resistance of a rear-face individual electrode pattern almost the same, it is lost that the driver voltage wave of a piezoelectric device varies by wiring resistance, the ink drop injection without dispersion is attained, and image quality improves.

[0079] Next, the 4th operation gestalt of this invention is explained with reference to drawing 16. In addition, this drawing is also explanatory drawing by the side of a substrate rear face. When thermocompression bonding is carried out with the arm head of the 1st operation gestalt mentioned above using solder when densification of 100 or more dpi is performed for example, the flash of a pewter arises on the edge of an electrode, and a contiguity electrode may be contacted and it may flow.

[0080] That is, when the nozzle configuration density of a single tier is 100 or more dpi, since it is set to 254 micrometers and the through hole also corresponds with it, the array dense pitch of a nozzle is set to 254 micrometers the same [the array pitch of a through hole]. When the rear-face individual electrode pattern 33 is formed in this by the line / space =127micrometer / 127 micrometers, there are only 127-micrometer inter-electrode gaps, to it, that of a pewter may produce the amount of headers to about 160 micrometers with about 80 micrometers and a both-sides electrode at the maximum, therefore contiguity electrodes may contact.

[0081] Then, in this operation gestalt, the rear-face individual electrode pattern 33 changed length by turns, and has arranged alternately surface-of-action 33a with FPC37. Therefore, surface-of-action 33a becomes possible [securing distance enough]. Thereby, even if there is a flash of hang, a contiguity electrode is not contacted and FPC mounting with sufficient reliability is attained.

[0082] In this case, also in the case of high density (300 or more dpi) which has only a space below the

amount of flashes of hang, it is lost by covering with the insulating resist 69 that contact of electrodes arises of surface-of-action 33a which adjoins as shown in this drawing, and the approaching rear-face individual electrode pattern 33.

[0083] Next, the 5th operation gestalt of this invention is explained with reference to drawing 17. In addition, this drawing is also explanatory drawing by the side of a substrate rear face. When thermocompression bonding is carried out with the arm head of said 1st operation gestalt using solder when densification of 100 or more dpi is performed for example, as mentioned above, the flash of a pewter arises on the edge of an electrode, and a contiguity electrode may be contacted and it may flow.

[0084] That is, when the nozzle configuration density of a single tier is 100 or more dpi, since it is set to 254 micrometers and the through hole also corresponds with it, the array dense pitch of a nozzle is set to 254 micrometers the same [the array pitch of a through hole]. When the rear-face individual electrode pattern 33 is formed in this by the line / space =127micrometer / 127 micrometers, there are only 127-micrometer inter-electrode gaps, to it, that of a pewter may produce the amount of headers to about 160 micrometers with about 80 micrometers and a both-sides electrode at the maximum, therefore contiguity electrodes may contact.

[0085] on the other hand -- the amount of the solder for connection -- being few (the thickness of a solder layer being thin) -- sufficient connection is not made but it becomes easy to produce a poor contact. Moreover, solder will overflow the polar zone greatly by application of pressure at the time of thermocompression bonding as there are too many amounts of solder (the thickness of a solder layer is thick). Therefore, although there is an optimum value in the thickness of solder, as it mentioned above to the case to connect with sufficient reliability, it is generated to about 160 micrometers with about a maximum of 80 micrometers and a both-sides electrode, and that contiguity electrodes contact produces the amount of flashes of a pewter.

[0086] Then, in this operation gestalt, the rear-face individual electrode pattern 33 is changing the direction of drawing every other through hole. Therefore, surface-of-action 33a becomes possible [securing distance enough]. Thereby, even if there is a flash of hang, a contiguity electrode is not contacted and FPC mounting with sufficient reliability is attained.

[0087] In this case, also in the case of high density (300 or more dpi) which has only a space below the amount of flashes of a pewter, it is lost by covering portions other than surface-of-action 33a and 35a with the insulating resist 69, as shown in drawing 18 that contact of electrodes arises.

[0088] Next, the 6th operation gestalt of this invention is explained with reference to drawing 19. Improvement in the speed of ink jet recording devices (image formation equipment is included), such as a printer, or when it colorizes, print with two or more arm heads of black ink, or **** will be performed with a multi-arm head called seven colors which added six colors and red (R) which added yellow (Y), a Magenta (M), cyanogen (C), four colors of black (K) or a thin Magenta, and cyanogen, green (G), and blue (B).

[0089] In this operation gestalt, two arm heads 81 are mounted in FPC82 of one sheet. Each arm head 81 is a configuration which a through hole is formed as mentioned above, and is connected with FPC82 in a rear face. Thus, by connecting with FPC with the rear face, FPC connection becomes easy, and since the width of face of an arm head may be small to necessary minimum, the miniaturization in the case of a multi-arm head is realizable. Of course, not only two arm heads but three more or more arm heads can also be formed on the same FPC.

[0090] In addition, in each above-mentioned operation gestalt, although the example which applied this invention to the piezo mold ink jet arm head which uses a piezoelectric device for an actuator means explains, it can also apply also to the bubble mold ink jet arm head using an exoergic resistor, and can apply also to the electrostatic type ink jet arm head using the electrostatic force between a diaphragm and the electrode which counters this.

[0091]

[Effect of the Invention] Since it considered as the configuration which established the connecting means which connects the fields and the pressure generating means other than the field in which the pressure generating means formed to the substrate which established the pressure generating means of

an ink-jet arm head, and prepared the connection pattern which connects with a printed circuit board in fields other than the field which formed this connecting means further according to the ink-jet recording device of claim 1 as having explained above, reliability improves, a drawer electrode section becomes short, and a miniaturization and low-cost-ization can plan.

[0092] Since the connecting means was considered as the configuration which connected the fields and pressure generating means other than the field in which the pressure generating means was formed through the breakthrough formed in the substrate, and prepared the connection pattern in the rear face of a substrate in the ink jet recording device of above-mentioned claim 1 according to the ink jet recording device of claim 2, reliability improves, a drawer electrode section becomes short, and miniaturization and low cost-ization can be attained.

[0093] Since it considered as the configuration which covered a part of field [at least] except the field which connects the pattern of a printed circuit board with the material which has insulation in above-mentioned claim 1 or the ink jet recording device of 2 according to the ink jet recording device of claim 3, while the inter-electrode short circuit at the time of printed circuit board mounting can be prevented and reliability improves, the yield improves and low cost-ization can be attained.

[0094] A miniaturization can be attained, while according to the ink jet recording device of claim 4 the inter-electrode short circuit at the time of printed circuit board mounting can be prevented and reliability improves in above-mentioned claim 1 thru/or one ink jet recording device of 3, since it considered as the configuration whose maximum array pitch of a connection pattern is more than an array pitch of a connecting means.

[0095] Since the connecting means considered as the configuration by which two or more trains arrangement is carried out in above-mentioned claim 1 thru/or one ink jet recording device of 4 according to the ink jet recording device of claim 5, reliability **** mounting can be performed and densification can be attained.

[0096] Since the inlet connection of the printed circuit board of a connection pattern considered as the configuration by which two or more trains arrangement is carried out in above-mentioned claim 1 thru/or one ink jet recording device of 5 according to the ink jet recording device of claim 6, reliability **** mounting can be performed and densification can be attained.

[0097] Since it considered as the configuration which the ink jet recording device of above-mentioned claim 1 set, has arranged two or more trains of pressure generating means, established the connecting means of two or more trains corresponding to each, and prepared inlet connection with a printed circuit board inside the connecting means according to the ink jet recording device of claim 7, the miniaturization of an arm head can be attained.

[0098] Since it considered as the configuration by which inlet connection with the printed circuit board of a connection pattern is stationed at the both sides of a connecting means in above-mentioned claim 1 thru/or one ink jet recording device of 7 according to the ink jet recording device of claim 8, reliability **** mounting can be performed and densification can be attained.

[0099] Since the connection pattern and the printed circuit board were considered as the configuration connected with the different direction electrical conducting material in above-mentioned claim 1 thru/or one ink jet recording device of 8 according to the ink jet recording device of claim 9, densification can be attained.

[0100] Since according to the ink jet recording device of claim 10 two or more ink jet arm heads were carried and at least two or more of ink jet arm heads of it considered as the configuration prepared on one printed circuit board in above-mentioned claim 1 thru/or one ink jet recording device of 9, the miniaturization of a multi-arm head can be attained.

[Translation done.]

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] The appearance perspective diagram showing an example of the ink jet head section of the ink jet recording device concerning the 1st operation gestalt of this invention

[Drawing 2] The decomposition perspective diagram of this ink jet arm head

[Drawing 3] The important section expanded sectional view which meets the A-A line of drawing 1

[Drawing 4] The important section expanded sectional view which meets the B-B line of drawing 1

[Drawing 5] The important section enlarged view of drawing 3

[Drawing 6] Rear-face explanatory drawing of the substrate of this arm head

[Drawing 7] Strabism explanatory drawing with which explanation of the manufacturing process of the actuator unit of this arm head is presented

[Drawing 8] Explanatory drawing showing other 1st example on the rear face of a substrate of this arm head

[Drawing 9] Explanatory drawing showing other 2nd example on the rear face of a substrate of this arm head

[Drawing 10] Explanatory drawing showing other 3rd example on the rear face of a substrate of this arm head

[Drawing 11] Strabism explanatory drawing with which explanation of the manufacturing process of the actuator unit of this arm head is presented

[Drawing 12] Strabism explanatory drawing with which explanation of the manufacturing process of the actuator unit of this arm head is presented

[Drawing 13] Rear-face explanatory drawing of the substrate with which explanation of the 2nd operation gestalt of this invention is presented

[Drawing 14] Rear-face explanatory drawing of the substrate with which explanation of the 3rd operation gestalt of this invention is presented

[Drawing 15] Rear-face explanatory drawing of the substrate with which explanation of other examples of this operation gestalt is presented

[Drawing 16] Rear-face explanatory drawing of the substrate with which explanation of the 4th operation gestalt of this invention is presented

[Drawing 17] Rear-face explanatory drawing of the substrate with which explanation of the 5th operation gestalt of this invention is presented

[Drawing 18] Rear-face explanatory drawing of the substrate with which explanation of other examples of this operation gestalt is presented

[Drawing 19] Strabism explanatory drawing with which explanation of the 6th operation gestalt of this invention is presented

[Description of Notations]

1 -- actuator unit, 2 -- liquid room unit, and 3 --- a substrate, 4 -- piezoelectric-device train, 5 -- frame member, and 7 --- a piezoelectric device, 12 -- diaphragm, 13 -- passage septum member, and 14 --- a nozzle, 15 -- nozzle plate, a 22 -- individual drawer electrode, and 23 --- a through hole electrode, a 24

-- common electrode, 25 -- through hole electrode, and 33 --- a rear-face individual electrode pattern, 35 -- rear-face common electrode pattern, and

[Translation done.]

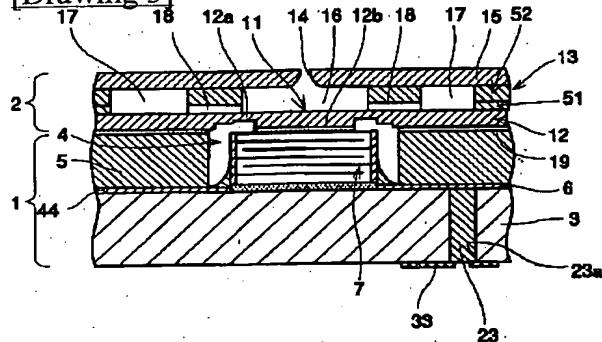
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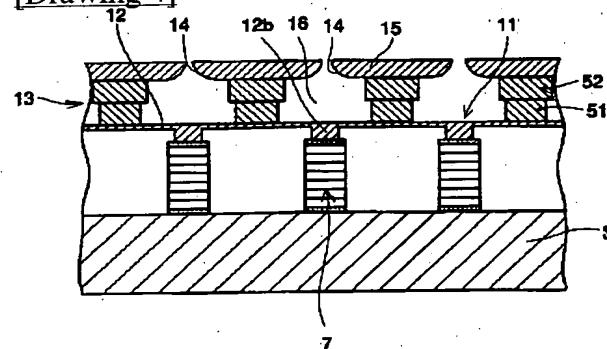
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DRAWINGS

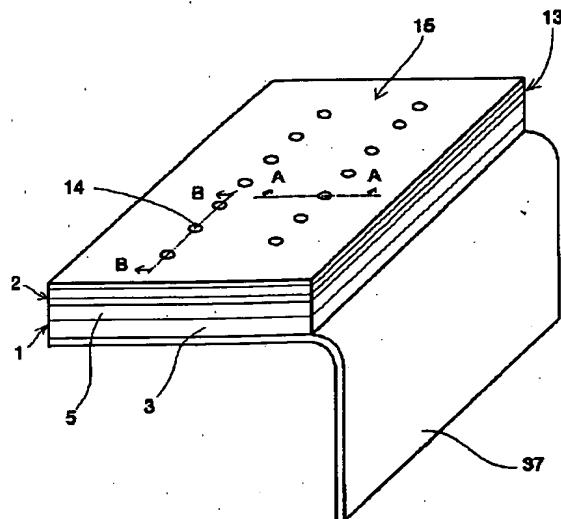
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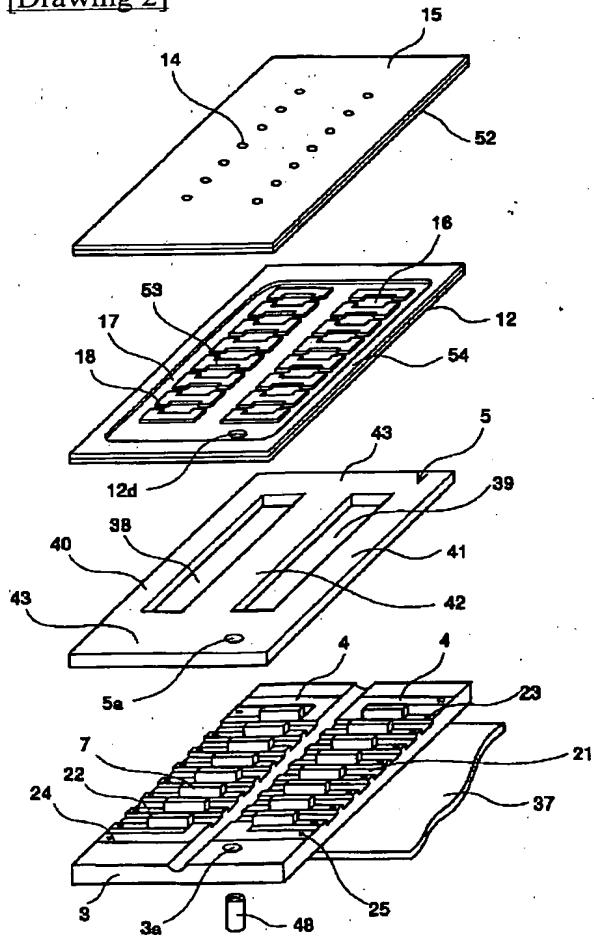
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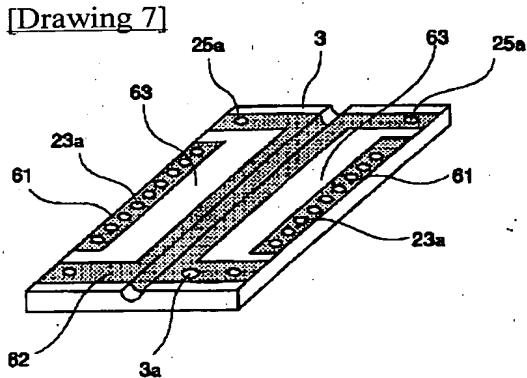
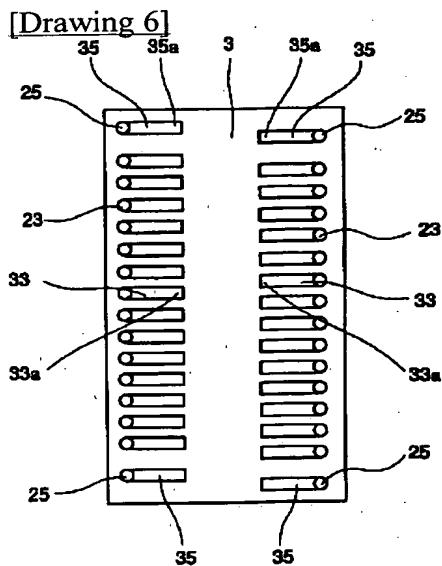
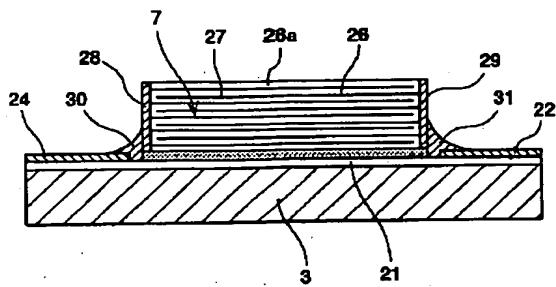
[Drawing 1]



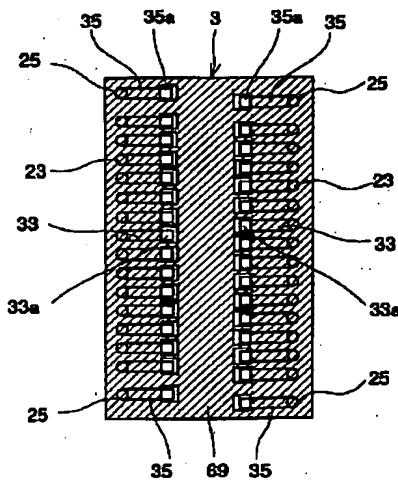
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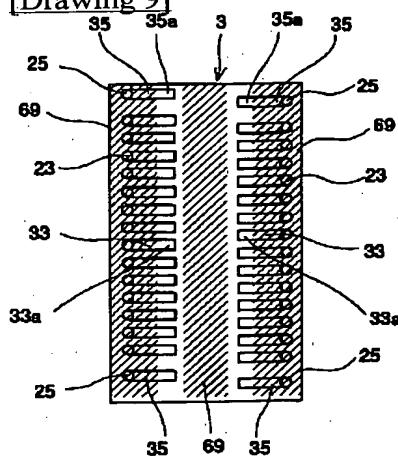
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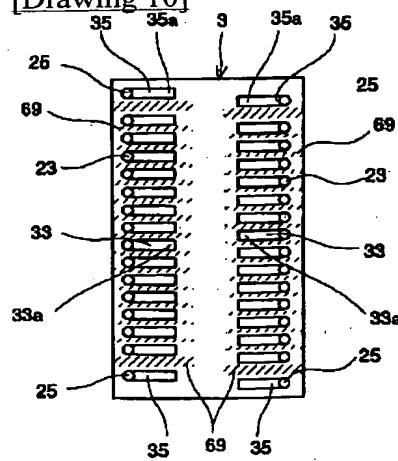
[Drawing 8]



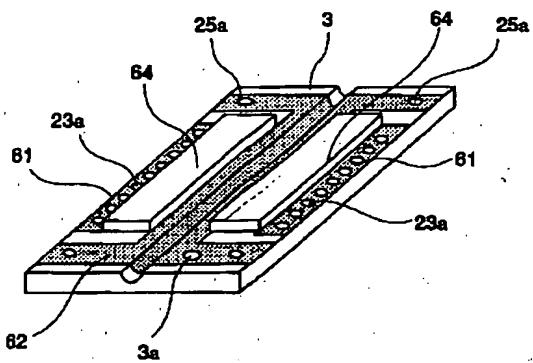
[Drawing 9]



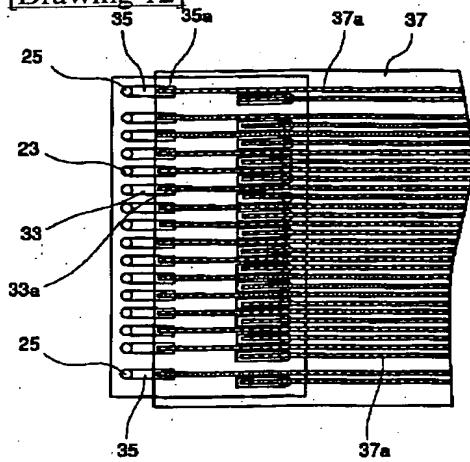
[Drawing 10]



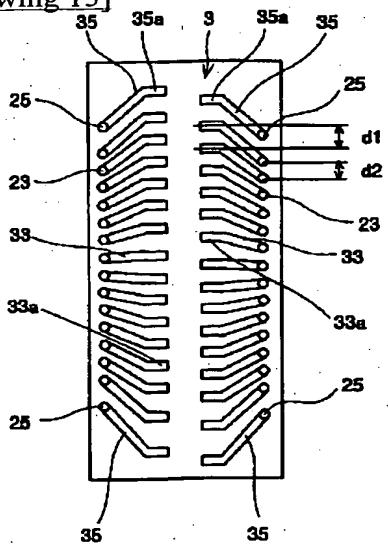
[Drawing 11]



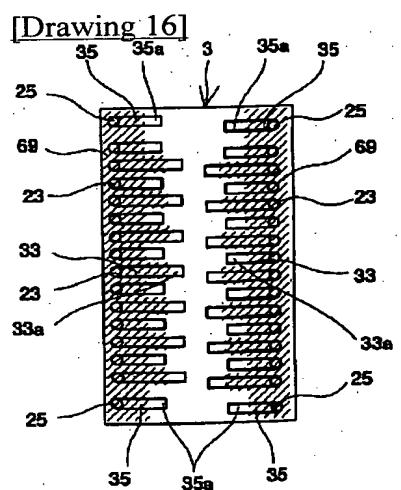
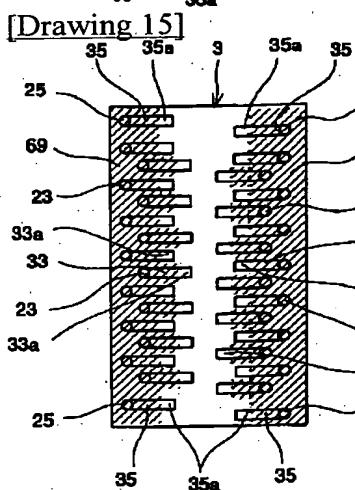
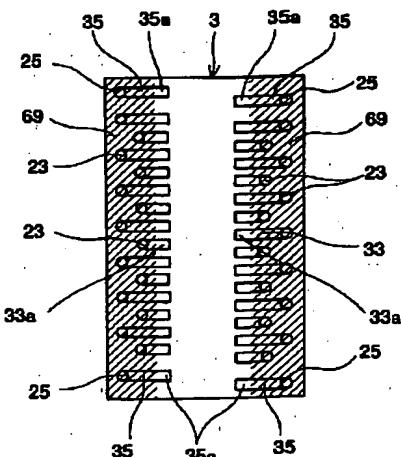
[Drawing 12]



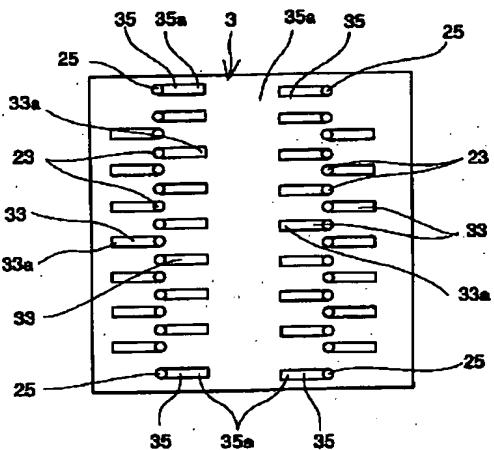
[Drawing 13]



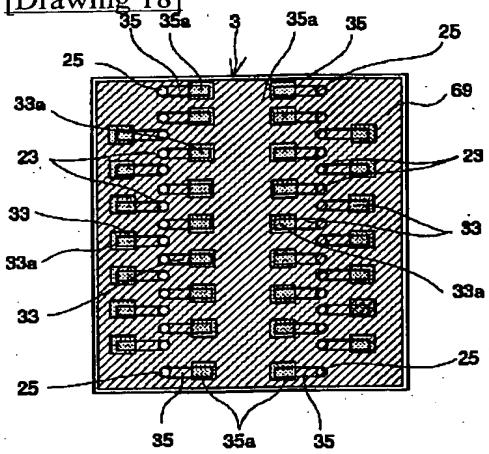
[Drawing 14]



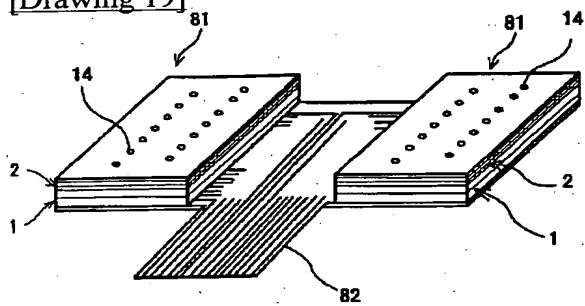
[Drawing 17]



[Drawing 18]



[Drawing 19]



[Translation done.]

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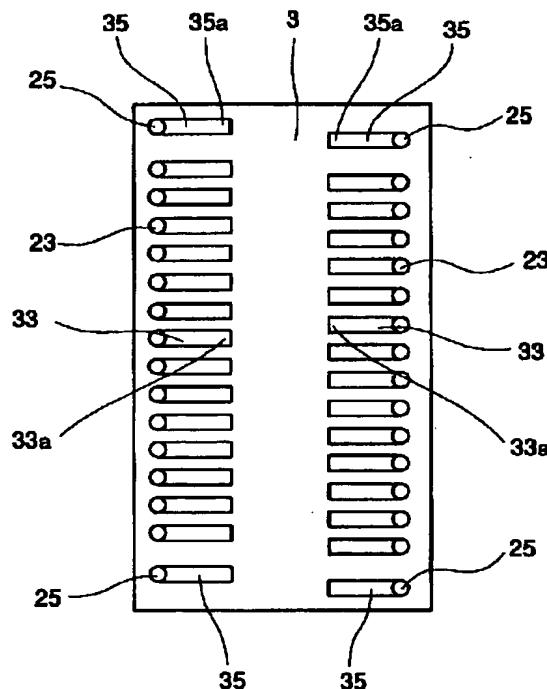
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(54)【発明の名称】 インクジェット記録装置

(57)【要約】

【課題】 高密度化、高信頼性、小型化、低コスト化が十分でない。

【解決手段】 基板3の圧電素子7を裏面に接続するスルーホール電極23、25を設け、このスルーホール電極23、25以外の領域でFPC37との接続部を有する裏面個別電極パターン33及び裏面共通電極パターン35を設けた。



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(P2000-263781A)

(2)

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【特許請求の範囲】

【請求項1】 インク滴を吐出するノズルと、このノズルが連通する液室と、この液室内容積を変化させる圧力を発生する圧力発生手段と、この圧力発生手段を基板に設けたインクジェットヘッドを搭載し、このインクジェットヘッドの前記圧力発生手段に駆動波形を印加するためのパターンが形成されたプリント基板を有するインクジェット記録装置において、前記基板には前記圧力発生手段を設けた面以外の面と前記圧力発生手段とを接続する接続手段を設け、更にこの接続手段を形成した領域以外の領域で前記プリント基板と接続する接続パターンを設けたことを特徴とするインクジェット記録装置。

【請求項2】 請求項1に記載にインクジェット記録装置において、前記接続手段は前記基板に形成した貫通孔を介して前記圧力発生手段を設けた面以外の面と前記圧力発生手段とを接続し、前記基板の裏面に前記接続パターンを設けたことを特徴とするインクジェット記録装置。

【請求項3】 請求項1又は2に記載のインクジェット記録装置において、前記プリント基板のパターンを接続する領域を除く領域の少なくとも一部を絶縁性を有する材料で被覆したことを特徴とするインクジェット記録装置。

【請求項4】 請求項1乃至3のいずれかに記載のインクジェット記録装置において、前記接続パターンの最大配列ピッチが前記接続手段の配列ピッチ以上であることを特徴とするインクジェット記録装置。

【請求項5】 請求項1乃至4のいずれかに記載のインクジェット記録装置において、前記接続手段が複数列配置されていることを特徴とするインクジェット記録装置。

【請求項6】 請求項1乃至5のいずれかに記載のインクジェット記録装置において、前記接続パターンの前記プリント基板との接続部が複数列配置されていることを特徴とするインクジェット記録装置。

【請求項7】 請求項1に記載のインクジェット記録装置において、前記圧力発生手段を2列以上配置し、それぞれに対応する2列以上の接続手段を設け、前記プリント基板との接続部を前記接続手段の内側に設けたことを特徴とするインクジェット記録装置。

【請求項8】 請求項1ないし7のいずれかに記載のインクジェット記録装置において、前記接続パターンのプリント基板との接続部が前記接続手段の両側に配置されていることを特徴とするインクジェット記録装置。

【請求項9】 請求項1ないし8のいずれかに記載のインクジェット記録装置において、前記接続パターンとプリント基板とを異方導電材料で接続したことを特徴とするインクジェット記録装置。

【請求項10】 請求項1乃至9のいずれかに記載のインクジェット記録装置において、複数のインクジェット

ヘッドを搭載し、そのうちの少なくとも2以上のインクジェットヘッドが1つのプリント基板上に設けられていることを特徴とするインクジェット記録装置。

【発明の詳細な説明】

【0001】

【産業上の利用分野】 本発明はインクジェット記録装置に関し、特にインクジェットヘッドとプリント基板との接続構造に関する。

【0002】

【従来の技術】 インクジェット記録装置は、記録時の振動、騒音が殆どなく、特にカラー化が容易なことから、コンピュータ等のデジタル処理装置のデータを出力するプリンタの他、ファクシミリやコピー機等にも用いられるようになっている。このようなインクジェット記録装置に用いられるインクジェットヘッドは、圧電素子（ピエゾ型）、発熱抵抗体（バブル型）、振動板と対向電極（静電型）等のアクチュエータ手段（圧力発生手段）を記録信号に応じて駆動して、ノズルからインク滴を吐出飛翔させて記録媒体上に画像記録を行なうものである。

【0003】 例えば、圧電素子を用いるインクジェットヘッドとしては、特開平8-142324号公報などに記載されているように、ヘッド基板上に複数の積層型圧電素子を複数列列状に接合して配設すると共に、圧電素子の周囲に位置するフレーム部材を接合し、これらの圧電素子及びフレーム部材上に、ダイアフラム部を有する振動板を積層し、この振動板上に積層型圧電素子でダイアフラム部を介して加圧される加圧液室及びこの液室にインクを供給するインク供給路を形成する液室隔壁部材を積層し、更にこの液室隔壁部材上にノズルを形成したノズルプレートを積層して、積層型圧電素子のd33方向の変位でノズルからインク滴を吐出させるようにしたものなどがある。

【0004】 このような圧電素子を用いるインクジェットヘッドにおいては、圧電素子と圧電素子に所要の駆動波形を印加するためのドライバ（駆動IC）を実装したプリント基板との間を電気的に接続する必要があり、従来、ワイヤボンディング法が用いられている（特開平6-320721号公報）。

【0005】 しかしながら、ワイヤボンディング法の場合、ヘッド側基板及びプリント基板側電極の電極材料を、例えば金メッキを使用しなければならないなど、選択する必要がある。また、1本1本順次接続するためには、高集積ノズル（例えば100ノズル以上）の場合は、ワイヤボンディング数が多くなり、作業時間が長く、コストも高くなる。さらに、ワイヤボンディング部はワイヤ同士の接触や、衝撃、異物の混入などによる断線から保護するために封止する必要があるなど、問題が多い。

【0006】 そこで、特開平6-320721号公報に開示されているように、圧電素子の電極とフレキシブル

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プリントケーブル（FPC）とを、直接ハンダ、異方導電テープで接続する方法がある。

【0007】また、フレキシブル配線板の接続方法としては、実開平5-28673号公報に開示されているように、周りに電極を配した板状圧電体を下基板と上基板とで挟み、一方の基板及び板状圧電体のそれぞれの周辺に複数個のスルーホール電極を穿設し、駆動電極とフレキシブル基板とをスルーホールを通して接続する方法が知られている。

【0008】

【発明が解決しようとする課題】ところが、上述した圧電素子とFPCとを直接接続する構造にあっては、FPCとの接続部（接触部、接触領域とも称する。）が基板面のノズルと同じ方向にあるため、インクが付着して電極間がリークするのを防止するための万全の保護をしなければならない。また、FPCとの接触部は流路板、共通液室板、ノズルプレートがなく、表面が露出している必要があるため、少なくとも接触部の長さ以上に圧電素子を余分に出す必要があって、圧電体の大きさが大きくなる。

【0009】また、スルーホールを用いる構造にあっては、圧電体と反対の基板面でフレキシブル基板と接続することができるために、インクによる汚染等を防止するための万全の保護や圧電体を大きくする必要がなくなるものの、基板にはスルーホールを形成するためにかなり凹凸が大きくなり、そのため、フレキシブル基板と、信頼性良く、歩留まり良く接続することが上記公報に開示されている限りでは不明である。

【0010】本発明は上記の点に鑑みてなされたものであり、搭載するインクジェットヘッドの高密度化、小型化、低コスト化、高信頼性を実現できるインクジェット記録装置を提供することを目的とする。 30

【0011】

【課題を解決するための手段】上記の課題を解決するため、請求項1のインクジェット記録装置は、インク滴を吐出するノズルと、このノズルが連通する液室と、この液室内容積を変化させる圧力を発生する圧力発生手段と、この圧力発生手段を基板に設けたインクジェットヘッドを搭載し、このインクジェットヘッドの前記圧力発生手段に駆動波形を印加するためのパターンが形成されたプリント基板を有するインクジェット記録装置において、前記基板には前記圧力発生手段を設けた面以外の面と前記圧力発生手段とを接続する接続手段を設け、更にこの接続手段を形成した領域以外の領域で前記プリント基板と接続する接続パターンを設けた構成とした。なお、「プリント基板」にはプリント基板（PCB）、フレキシブルプリントケーブル（FPC）、導電性フィルムなどを含む意味で用いる。

【0012】請求項2のインクジェット記録装置は、上記請求項1のインクジェット記録装置において、前記接

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続手段は前記基板に形成した貫通孔を介して前記圧力発生手段を設けた面以外の面と前記圧力発生手段とを接続し、前記基板の裏面に前記接続パターンを設けた構成とした。

【0013】請求項3のインクジェット記録装置は、上記請求項1又は2のインクジェット記録装置において、前記プリント基板のパターンを接続する領域を除く領域の少なくとも一部を絶縁性を有する材料で被覆した構成とした。

10 【0014】請求項4のインクジェット記録装置は、上記請求項1乃至3のいずれかのインクジェット記録装置において、前記接続パターンの最大配列ピッチが前記接続手段の配列ピッチ以上である構成とした。

【0015】請求項5のインクジェット記録装置は、上記請求項1乃至4のいずれかのインクジェット記録装置において、前記接続手段が複数列配置されている構成とした。

20 【0016】請求項6のインクジェット記録装置は、上記請求項1乃至5のいずれかのインクジェット記録装置において、前記接続パターンの前記プリント基板との接続部が複数列配置されている構成とした。

【0017】請求項7のインクジェット記録装置は、上記請求項1のインクジェット記録装置において、前記圧力発生手段を2列以上配置し、それぞれに対応する2列以上の接続手段を設け、前記プリント基板との接続部を前記接続手段の内側に設けた構成とした。

【0018】請求項8のインクジェット記録装置は、上記請求項1乃至7のいずれかのインクジェット記録装置において、前記接続パターンのプリント基板との接続部が前記接続手段の両側に配置されている構成とした。

【0019】請求項9のインクジェット記録装置は、上記請求項1乃至8のいずれかのインクジェット記録装置において、前記接続パターンとプリント基板とを異方導電材料で接続した構成とした。

【0020】請求項10のインクジェット記録装置は、上記請求項1乃至9のいずれかのインクジェット記録装置において、複数のインクジェットヘッドを搭載し、そのうちの少なくとも2以上のインクジェットヘッドが1つのプリント基板上に設けられている構成とした。

【0021】

【発明の実施の形態】以下、本発明の実施の形態について添付図面を参照して説明する。以下、本発明の実施の形態を添付図面を参照して説明する。図1は本発明の第1実施形態に係るインクジェット記録装置のインクジェットヘッド部の一例を示す外観斜視図、図2は同インクジェットヘッドの分解斜視図、図3は図1のA-A線に沿う要部拡大断面図、図4は図1のB-B線に沿う要部拡大断面図、図5は図3の要部拡大図、図6は基板の裏面図である。

【0022】このインクジェットヘッドは、アクチュエ

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ータユニット1と、このアクチュエータユニット1上に接合した液室ユニット2とからなる。アクチュエータユニット1は、絶縁性の基板3上に複数の積層型圧電素子を列状に配置(列設)してなる2列の圧電素子列4、4及びこれら2列の圧電素子列4の周囲を取り囲むフレーム部材5を接着剤6によって接合している。圧電素子列4は、インクを液滴化して飛翔させるための駆動パルスが与えられる複数の圧電素子7で構成している。

【0023】液室ユニット2は、ダイアフラム部11を形成した振動板12上に加圧液室、共通インク流路等を形成する感光性樹脂フィルム(ドライフィルムレジスト)或いはSUSなどの金属プレートからなる流路隔壁部材13をドライフィルムレジストの熱圧着、或いは接着剤で接着し、この流路隔壁部材13上に複数のノズル14を形成したノズルプレート15を接着してなる。

【0024】これらの振動板12、流路隔壁部材13及びノズルプレート15によって各圧電素子列4の圧電素子7に対向するダイアフラム部11を有するそれぞれ略独立した複数の加圧液室16、各加圧液室16の両側に配置した共通液室17及び共通液室17から加圧液室16にインクを供給するインク供給路となる流体抵抗部18を形成し、かつ加圧液室16に連通するノズル14を各圧電素子7に対向して配置している。そして、この液室ユニット2はその振動板12が接着剤によってアクチュエータユニット1に高い剛性で接合している。

【0025】ここで、アクチュエータユニット1の基板3は、厚さ0.5~5mm程度で、しかも圧電素子に似た材質のものからなり、圧電素子と共に例えばダイヤモンド砥石による切削が可能なものであることが好ましく、また、圧電素子7に対応して高密度でスルーホールを形成できることが好ましい。

【0026】この基板3の圧電素子7の列設方向と直行する方向の両端部には各圧電素子列4の個々の圧電素子7の対向しない端面側を接続するスリット溝21で分割された各圧電素子7に選択信号を与えるための個別引出電極22を形成し、それぞれの個別引出電極22は接続手段であるスルーホール電極23を介して基板3の裏面側に接続している。また、各圧電素子列4、4間には各圧電素子に駆動波形を与えるための共通電極24を形成し、共通電極24は接続手段であるスルーホール電極25を介して基板3の裏面側に接続している。

【0027】ここで、圧電素子7と個別引出電極22及び共通電極24との位置関係は、図5に示すように、僅かに隙間を空けている。これは、圧電素子7が各電極22、24上に載ると、電極22、24の厚みや誤差が圧電素子7の接合品質、すなわち接合の均一性や接合後の面平行精度に影響を与えることになって好ましくないからである。ただし、圧電素子7と個別引出電極22及び共通電極24とが僅かにオーバラップする程度であれば悪影響は少ない。

【0028】また、圧電素子4は、図3及び図5に示すように10層以上の積層型圧電素子からなり、厚さ20~50μm/1層のPZT(=Pb(Zr-Ti)O₃)26と、厚さ数μm/1層の銀・バラジューム(AgPd)からなる内部電極27とを交互に積層したものである。そして、圧電素子7の最上層26aの上面には内部電極26に相当する電極を形成しないで不活性層としている。なお、圧電素子として用いる材料は上記に限られるものでなく、一般に圧電素子材料として用いられるBaTiO₃、PbTiO₃、(NaK)NbO₃等の強誘電体などを用いることもできる。

【0029】そして、各圧電素子列4の圧電素子7の多数の内部電極27を1層おきに交互に両端面に取り出して、両端面に形成した例えばAgPdからなる個別端面電極28、29に接続し、各圧電素子列4の各圧電素子7の対向する端面側の個別端面電極28を基板3上の共通電極24にヤング率200kgf/mm²以上の導通処理材料30を介して接続し、各圧電素子列4の各圧電素子7の対向しない端面側の個別端面電極29を基板3上の個別引出電極22に導通処理材料31を介して接続している。

【0030】各個別引出電極22及び共通電極24は、図6に示すように、それぞれスルーホール電極23、25を介して接続パターンである裏面個別電極パターン33及び裏面共通電極パターン35に導通させ、それぞれのFPC37との接続領域(接続部、接触部)で、プリント基板であるFPC37を接続されて(図1参照)、駆動電圧を与えられることによって積層方向に電界が発生して、圧電素子7には積層方向の伸びの変位(電界と同方向のd33方向の変位)が生起される。

【0031】フレーム部材5は、線膨張係数が2×10⁻⁶/℃以下のエポキシ樹脂系の熱硬化性成形材料からなる板状部材であって、圧電素子列4に対応する透孔部38、39を穿設して、各圧電素子7の列設方向と直交する方向の一方側に固定部40、41を形成すると共に、2つの圧電素子列4の他方側である中央部にも固定部42を形成し、これらの固定部40~42の各圧電素子7の列設方向の両端部に架橋部43を形成したものである。なお、フレーム部材5の一方の架橋部43には基板3のインク供給孔3aに対応するインク供給孔5aが形成されている。

【0032】そして、このフレーム部材5の固定部42下面には、図3に示すように導電性ペースト(導電性接合剤)44を全面に塗布して、スリット溝21で個々の圧電素子7(各チャンネル)毎に分割された共通電極24を相互に接続して、一体の共通電極24を形成している。

【0033】次に、液室ユニット2の振動板12は、図3に示すように加圧液室16側は平坦面とし、圧電素子列4側はそれぞれ厚みの異なるダイアフラム領域12

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a、接合領域12bを形成して、圧電素子列4の圧電素子7に対応してダイアフラム部11を形成したものである。この振動板12はNi(ニッケル)の金属プレートからなり、エレクトロフォーミング法によって製造している。なお、振動板12にもインク供給孔12dを形成している。

【0034】流路隔壁部材13は、振動板12上面とノズルプレート15との間に位置して加圧液室16の流路等を形成するものであり、その製造工程から下側流路隔壁部材51及び上側流路隔壁部材52で構成している。 10

【0035】下側流路隔壁部材51は、振動板12上面に接着された感光性樹脂フィルムまたはSUS基板からなり、図3に示すように上側流路隔壁部材52と相接つて圧電素子列4の各圧電素子7に対応して各々独立した加圧液室16等の流路を形成すると共に、各加圧液室16へのインク供給路を兼ねた流体抵抗部18を形成する多数の内側隔壁部53と、加圧液室16の周囲に共通液室17を形成する外周隔壁部54とからなる。上側流路隔壁部材52は、下側流路隔壁部材51と略同様の構成であるが、下側流路隔壁部材51の流体抵抗部18に相当する部分がない点で異なる。 20

【0036】ノズルプレート15にはインク滴を飛翔させるための微細孔である多数のノズル14が形成されており、このノズル14の径はインク滴出口側の直径で50μm以下に形成し、かつノズル14は加圧液室16の中心近傍に対応する位置に設けている。このノズルプレート15も振動板12と同様にNiの金属プレートからなり、エレクトロフォーミング法によって製造している。 30

【0037】なお、本実施形態では、加圧液室16の両側に共通液室17を設け、両側からインク供給を行なう例を示したが、共通液室、流体抵抗部を一方だけに設け、片側からインク供給する構成でもよい。また、ノズルの位置は特に中央に限つたものではなく、加圧液室の端部近傍に設けても良い。 30

【0038】次に、このインクジェットヘッドの製造工程について説明する。このインクジェットヘッドは、予めアクチュエータユニット1と液室ユニット2とを別々に組み付けた後、両ユニット1、2を接着接合して製造している。このような製造工程を採用することによって、両ユニット1、2の良品同士を選んで組み付けることができて歩留りが向上すると共に、加工組付け工程で塵等が発生しやすいアクチュエータユニット1と、塵等の付着を完全に避けたい液室ユニット2とを別々の工程で組付けることができるので、完成したインクジェットヘッドの品質自体が向上する。 40

【0039】以下、具体的に説明する。先ず、アクチュエータユニット1の加工及び組付け工程は、次のとおりである。すなわち、図7に示すように、セラミックス、高剛性の樹脂等の電気絶縁性材料から形成した基板3に 50

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予めインク供給孔3aを形成する。さらに、個別引出電極となる位置及び共通電極を形成する位置の一部に、スルーホール23a、25aを形成する。

【0040】そして、この基板3の両側部分に個別引出電極22を形成するための導電性材料からなる個別引出電極用パターン61を形成すると共に、基板3中央及び個別引出電極用パターン61を迂回して基板3の両端部に臨むように導電性材料からなる共通電極用パターン62を形成し、個別引出電極用パターン61と共に共通電極用パターン62との間を圧電素子接合領域63とする。さらに、個別引出電極用パターン61と共に共通電極用パターン62の形成と同時に、又は、それらを形成した後に、スルーホール23a、25a内部壁にも導電性材料からなる層を形成しておいても良い。

【0041】また、この基板3の裏面には、図6に示すように、個別引出電極22のスルーホール電極23からFPC37との接続部まで裏面個別電極パターン33を、共通電極25のスルーホール電極25からFPC37との接続部まで裏面共通電極パターン35を形成する。その後、スルーホール23a、25aにAgなどの通電性の良い材料を充填し、スルーホール電極23、25を形成する。充填方法は、Agをペースト状にして、スルーホール23a、25a内部に注入し、乾燥、固化させることで容易に行なえる。

【0042】さらに、少なくとも基板3の裏面の裏面個別電極パターン33と裏面共通電極パターン35のFPC37との接続部を除く部分を、感光性樹脂などの絶縁性で、パターン形成が容易な材料で被覆することが好ましい。これは、FPC37の接続時に、半田のはみ出しや飛び散りで電極間同士が接触するのを防止し、より信頼性のあるFPC実装を行うためである。

【0043】例えば、感光性樹脂69による被覆パターンとしては、図8に示すようにFPC37との接続領域33a、35aを除く部分以外を全面覆つてもよいし、図9に示すように各列のFPCとの接続領域33a、35a以外の部分を覆つても良く、或いは、図10に示すように隣接するFPC接続領域33a、35a間のみを覆つても良い。

【0044】また、接続パターンである裏面個別引出電極パターン33及び裏面共通電極パターン35のFPC接続領域33a、35aは、図6に示すようにスルーホール23a、25aの位置より、基板3の内側に形成する。これにより、FPC37との接続部を形成するために基板3が大きくなることがなく、ヘッドの小型化を図れる。

【0045】これらの各電極(電極パターン)22、24、33、35は、例えばNi、Au、Cu等の金属蒸着、又は同種金属の電解、無電界メッキ、あるいはAgPd、AgPt、Auペースト等の厚膜導体ペーストの印刷等の方法によって形成して基板3面に密着させている。

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【0046】そして、図11に示すように基板3上の前記圧電素子接合領域63に積層型圧電素子をプレート状（又はシート状）に形成してなる圧電素子プレート64を接着剤（図3参照）を用いて接着接合する。この圧電素子プレート64の基板3への接合に用いる接着剤としてはヤング率 200 kgf/mm^2 以上のものがよく、ここでは加熱硬化型のエポキシ系接着剤を使用している。接着剤の形態としては、1液タイプ、2液混合タイプ、フィルムタイプ等のいずれでも使用可能である。

【0047】そして、これらの圧電素子プレート64の10短辺部端面には予め個別端面電極（個別外部電極）28、29を形成するための端面電極を形成しておき、基板3上への接着接合後、これらの2枚の圧電素子プレート64の対向する側の端面電極を基板3上の共通電極用パターン62に導通処理材料30にて電気的に接続すると共に、2枚の圧電素子プレート64の対向しない端面電極を基板3上の各個別引出電極用パターン61に導通処理材料31にて電気的に接続する。この導通処理材料30、31としてはヤング率 200 kgf/mm^2 以上のものを用いている。また、導通処理材料としては、例え20ば導電性接着剤、Au等のスペッタリング、Au等の蒸着、AgPd等のデイッピングなどを用いることができる。

【0048】次いで、ダイヤモンド砥石をセットしたダイヤー等によって、2枚の圧電素子プレート64及び基板3の表面部を、その端面電極と直交する方向に所定のピッチ、例えは1ピッチ当たり $100\mu\text{m}$ 程度の幅の圧電素子7が形成されるピッチで切断するスリット加工を施して、複数の積層型圧電素子7を分割形成する同時に、端面電極を個々の圧電素子7に対応する個別端面電極28、29に分割する。

【0049】このとき、図5にも示すように基板3に所定の深さまで切込んでスリット溝21を入れて切断することによって、個々の圧電素子7を完全に独立させると共に、個別引出電極用パターン61を個々の圧電素子7にそれぞれ個別的に対応する個別引出電極22に分割する。この場合、基板3上の共通電極用パターン62もその一部が個々の圧電素子7に対応して分割されることになる。

【0050】なお、分割形成された個別引出電極2240は、個々の圧電素子7の対向しない端面側の個別端面電極29と導電処理材料31を介して接続されたままである。また、共通電極用パターン62も各圧電素子列4の圧電素子7の対向する端面側の個別端面電極28と導電処理材料30を介して接続されたままである。

【0051】このように、絶縁性基板3上に、引出電極用パターン61を形成すると共に、予め内部電極27を交互に両端面に取り出して各端面に形成した端面電極に導通接続した積層型圧電素子64を接合し、引出電極用パターン61と積層型圧電素子64の端面電極とを導通50

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処理して接続した後、積層型圧電素子64及び基板3の表面部に同時にスリット加工を施して、複数の圧電素子7を形成すると共に、引出電極用パターン61及び端面電極を複数の圧電素子7にそれぞれ個別的に対応する個別引出電極28及び個別端面電極29に分割することによって、複数の圧電素子の高密度集積化が図れ、内部電極27からの電極の取出しが容易になる上、圧電素子と基板が接合されて接合強度が高くなっているため、スリット加工時の圧電素子の破損が低減して、歩留りが向上し、コストの削減を図ることができる。

【0052】そして、積層型圧電素子の端面電極と基板上の引出電極とを導通させる導通処理材料30、31としてヤング率 200 kgf/mm^2 以上のものを用いることによって、圧電素子と基板との振動を低減することができて、スリット加工時の積層型圧電素子の破損が一層少なくなる。また、基板3と圧電素子7との接着剤としてヤング率 200 kgf/mm^2 以上のものを用いることによって、積層型圧電素子と基板との振動を低減することができ、スリット加工時の圧電素子の破損を少なくすることができると共に、圧電素子7の駆動時の変位効率の低下を防止してヘッドの特性を向上できる。

【0053】このようにして、圧電素子プレート64等のスリット加工が終了した基板3上にフレーム部材5をヤング率 200 kgf/mm^2 以上の加熱硬化型エポキシ系接着剤からなる接着剤を用いて接着接合する。このとき、このフレーム部材5の固定部42の裏面に導電性ペースト44を塗布することによってスリット加工で分割された共通電極形成用パターン62を相互に接続して、共通電極24を形成する。

【0054】ここで、フレーム部材5を接合した後のフレーム部材5上面と圧電素子7上面とは、精度良く同一平面となっている必要がある。これは、後述するようにこの部分に液室ユニット2の振動板12を接合するため、面精度が悪いと接着されないダイアフラム部11が発生するからである。

【0055】そこで、圧電素子7の最上層26aの上面に電極を形成しないで不活性層として表面加工を可能にし、圧電素子7の高さよりも僅かに高いフレーム部材5を接着接合した後、表面の研削加工を行い、圧電素子7の上面が僅かに削れて同一平面になるまで研削を行うようにして、両部品の寸法精度及び接着工法の困難性を解消している。

【0056】そして、このようにして完成したアクチュエータユニット1上に、別途加工組付けを行った液室ユニット2をその振動板12側（接合面）を下方にして、位置合わせしながら接着接合する。

【0057】その後、図12に示すように、基板3裏面の裏面個別電極パターン33及び裏面共通電極パターン35のスルーホール部を除く一部を接続領域33a、35aとして、FPC37の電極パターン37aを熱と加

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圧で接合する。なお、FPC37は圧電素子列4の圧電素子7を選択的に駆動できるパターンを有し、その接合部には予め半田メッキを施している。この場合、FPC37を熱圧着する時の温度は、半田の溶融温度以上が必要で、通常200°C以上である。

【0058】ここで、スルーホール電極23、25は、例えば、金属線などの電気伝導性の良い材料を予めセラミックスの中に配列し、焼成することで作ることができると、この方法は、加工が難しく、かつ、所望の配列を精度良く実現することが難しい。

【0059】そこで、基板3にドリルなどで穿孔して作る方法を用いる。これは、基板3に貫通孔（スルーホール）23a、25aをドリルで作製し、それに金属などの電気伝導性の良い材料を貫通孔内壁に形成したり、あるいはその材料を充填することで作製する。この方法は、比較的精度良く所望の位置に、所望の大きさの貫通孔を形成でき、しかも低コストであるという点で、優れている。

【0060】ただし、この方法では、スルーホールの周囲にバリが多く発生するため、スルーホール部は基板の凹凸が激しくなり、この部分でハンダを熱圧着した場合には、接触不良が生じ易くなる。そこで、本発明では、スルーホールから電極パターンを形成して、スルーホールを避けて、比較的フラットな基板部分で熱圧着することで信頼性の良いFPC実装が可能になる。

【0061】また、FPCと裏面個別電極パターン及び裏面共通電極パターンとの電気的接続方法としては、半田以外に、異方導電性フィルムを用いることもできる。異方導電性フィルムは、熱硬化性、あるいは熱可塑性樹脂フィルムの中に、フィラーと呼ばれる導電性粒子（金屬粒子やカーボン粒子）を分散させたもので、裏面個別電極パターン及び個別共通電極パターンとFPCの間に、異方導電性フィルムを挟んで、加熱、加圧することにより、フィラーを通じて裏面個別電極パターン及び裏面共通電極パターンとFPCの電極が導通する。異方導電性フィルムの場合でも、同様にスルーホール以外のフラットな部分で熱圧着することで、信頼性が向上する。

【0062】さらに、半田接続方法が電極部の半田のみで基板3とFPC37とが固定されるのに対して、異方導電性フィルムの場合、電極部はもちろんあるが、電極が形成されていない部分でも、異方導電性フィルムの樹脂が接着剤となって、基板3とFPC37を固定するので、接着強度を得る上ではより好ましい。また、150°C以下で熱圧着が可能であるため、FPC37を加熱、加圧することによりFPC37の樹脂基板が熱膨張～収縮して生じる応力の発生が、低減されて、電極の剥がれなどがなく、好ましい。

【0063】このようにしてFPC37を実装した後に、最後に、基板3のインク供給孔3aにインク供給パイプ48を挿入して接着剤を塗布硬化して固定する。

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【0064】ここで、アクチュエータユニット1のフレーム部材5を線膨張係数が 2×100^{-6} / °C以下のエポキシ樹脂系の熱硬化性成形材料から形成しているので、液室ユニット2の振動板12とフレーム部材5とを接着接合するときに、加熱接着をしても振動板12の変形を来さない。このようにフレーム部材5と液室ユニット2とを加熱接着することができるので、組立性が向上し、コストも低減する。

【0065】また、上述したように、基板3とフレーム部材5、アクチュエータユニット1と液室ユニット2、圧電素子7と基板3とを接合する接着剤として、ヤング率が200 kgf/mm²以上で、同一のエポキシ系加熱硬化型接着剤を用いることによって、コストが低減する。

【0066】次に、以上のように構成したインクジェットヘッドの作用について説明すると、記録信号に応じて選択的に圧電素子7に20～50Vの駆動パルス電圧を印加することによって、パルス電圧が印加された圧電素子7が変位して振動板12の対応するダイアフラム部11をノズル14方向に変形させ、加圧液室16の容積（体積）変化によって加圧液室16内のインクを加圧し、インクがノズルプレート15のノズル14から液滴となって噴射され、記録を行うことができる。

【0067】そして、インク滴の吐出に伴って加圧液室16内のインク圧力が低下し、このときのインク流れの慣性によって加圧液室16内には若干の負圧が発生する。この状態の下において、圧電素子7への電圧の印加をオフ状態にすることによって、振動板12のダイアフラム部11が元の位置に戻って加圧液室16が元の形状になるため、さらに負圧が発生する。このとき、図示しないインクタンクに通じるインク供給パイプ48から入ったインクは、共通液室27を通って流体抵抗部28から加圧液室16内に充填される。そこで、ノズル14のインクメニスカス面の振動が減衰して安定した後、次のインク滴吐出のために圧電素子7にパルス電圧を印加する。

【0068】なお、上記実施形態においては、圧電素子7の両端面の個別端面電極28、29と共通電極24、個別引出電極22とを導通処理する導通処理材料30、31は個別端面電極28、29の外面の一部に付着させているが、導通処理材料30、31を個別端面電極28、29の全面に付着させて導通処理を行うことによって、圧電素子7となる前の圧電素子プレート64に対するスリット加工前の圧電素子プレート64と基板3との接合強度を飛躍的に向上させることができ、スリット加工時の積層型圧電素子の破損を一層低減することができる。

【0069】また、上記実施形態においては、ノズルの開口方向を圧電素子の変位方向と同軸上にしたサイドシュー方式のインクジェットヘッドに適用した例で説明

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したが、ノズルの開口方向を圧電素子の変位方向と直交する方向にしたエッジシュータ方式のインクジェットヘッドにも適用することができる。さらに、本実施形態においては、プリント基板としてFPCを用いたが、可撓性のないリジッドな基板（いわゆるPCB基板）を用いても同様の効果があるが、リジッド基板の場合圧電素子側で接続すると、基板の厚さが厚いため、ノズル面より基板が高くなってしまうという不具合が生じるので、さらに本発明が有効になる。

【0070】次に、本発明の第2実施形態について図13を参照して説明する。なお、同図は基板裏面側の説明図である。上述した第1実施形態のヘッドで、100dpi以上の高密度化を行なった場合、例えば半田を用いて熱圧着すると、電極の縁にハンダのはみ出しが生じ、隣接電極と接触して導通してしまうことがある。

【0071】すなわち、一列のノズル配列密度が100dpi以上の場合、ノズルの配列密ピッチは254μmとなり、スルーホールもそれと対応しているため、スルーホールの配列ピッチも同じく254μmになる。これに例えば、ライン/スペース=127μm/127μmで裏面個別電極パターン33を形成した場合、電極間の間隔は127μmしかなく、それに対して、ハンダのはみ出しが最大で80μm程度、両側電極で160μm程度まで生じることがあり、そのために、隣接電極同士が接触してしまうことがある。

【0072】そこで、本実施形態においては、裏面個別電極パターン33は、個別電極用スルーホール23aを最狭部として広がりを持たせ、先端部にFPC37との接触領域33aを設けている。

【0073】したがって、接触領域33aにおける裏面個別電極パターンのピッチd1は、個別電極用スルーホール23aのピッチd2より大きくなる（d1>d2）。これにより、ハンダのはみ出しがあっても、隣接電極同士が接触することがなくなり、信頼性のよいFPC実装が可能となる。

【0074】次に、本発明の第3実施形態の異なる例について図14及び図15を参照して説明する。なお、両図も基板裏面側の説明図である。上述した第1実施形態のヘッドで、100dpi以上の高密度化を行なった場合、スルーホールを1列で形成すると、スルーホールの径を小さくすることに限界があり、スルーホール間の壁が少ないと、スルーホール形成時に、壁部分でクラックが入ったり、最悪の場合には壁がなくなりスルーホール同士がつながったりすることがある。

【0075】そこで、本実施形態においては、裏面個別電極パターン用のスルーホール23aを千鳥状に配列して形成されている。これによって、スルーホール同士は十分距離を確保することができる、クラックの発生や、スルーホール同士の連通などを防止することができ、信頼性が

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向上する。

【0076】ここで、FPC37との接触領域33aは、図14に示すように1列に形成してもよく、或いは、図15に示すようにスルーホールと同様に千鳥状に配列してよい。

【0077】接触領域を1列に形成した場合には、接触領域を一括してFPCと熱圧着することができ、FPCを加熱、押圧するための圧着装置の加熱押圧ヘッドの幅が狭くてよくなり、加熱押圧ヘッドの温度ムラが少なくなるので、すべての接触領域で、ばらつきの少ない信頼性の高い接続を行うことができる。また、押圧面積が小さくなるので、熱圧着に必要な圧力を得るための圧着装置の加圧力が小さくてよくなり、熱圧着装置自体の小型、低価格化を図ることができる。

【0078】一方、接触領域をスルーホールと同様の千鳥状配列とした場合には、スルーホールと接触領域との間の裏面個別電極パターンの長さをほぼ同じに揃えることができるので、裏面個別電極パターンの配線抵抗をほぼ同じにすることことができ、圧電素子の駆動電圧波形が配線抵抗によってばらつくことがなくなり、ばらつきのないインク滴噴射が可能になり、画質が向上する。

【0079】次に、本発明の第4実施形態について図16を参照して説明する。なお、同図も基板裏面側の説明図である。上述した第1実施形態のヘッドで、100dpi以上の高密度化を行なった場合、例えば半田を用いて熱圧着すると、電極の縁にハンダのはみ出しが生じ、隣接電極と接触して導通してしまうことがある。

【0080】すなわち、一列のノズル配列密度が100dpi以上の場合、ノズルの配列密ピッチは254μmとなり、スルーホールもそれと対応しているため、スルーホールの配列ピッチも同じく254μmになる。これに例えば、ライン/スペース=127μm/127μmで裏面個別電極パターン33を形成した場合、電極間の間隔は127μmしかなく、それに対して、ハンダのはみ出しが最大で80μm程度、両側電極で160μm程度まで生じることがあり、そのために、隣接電極同士が接触してしまうことがある。

【0081】そこで、本実施形態においては、裏面個別電極パターン33は、交互に長さを異なさせて、FPC37との接触領域33aを千鳥状に配列している。したがって、接触領域33a同士は十分距離を確保することができる。これにより、ハングのはみ出しがあっても、隣接電極と接触する事がなく、信頼性のよいFPC実装が可能になる。

【0082】この場合、同図に示すように隣接する接触領域33aと近接する裏面個別電極パターン33は絶縁性のレジスト69で被覆することによって、ハングのはみ出しが最大で80μm程度、両側電極で160μm程度まで生じることがあり、そのために、隣接電極同士が接触してしまうことがある。

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【0083】次に、本発明の第5実施形態について図17を参照して説明する。なお、同図も基板裏面側の説明図である。上述したように、前記第1実施形態のヘッドで、100dpi以上の高密度化を行なった場合、例えば半田を用いて熱圧着すると、電極の縁にハンダのはみ出しが生じ、隣接電極と接触して導通してしまうことがある。

【0084】すなわち、一列のノズル配列密度が100dpi以上の場合、ノズルの配列密ピッチは $254\mu\text{m}$ となり、スルーホールもそれと対応しているため、スルーホールの配列ピッチも同じく $254\mu\text{m}$ になる。これに例え、ライン/スペース= $127\mu\text{m}/127\mu\text{m}$ で裏面個別電極パターン33を形成した場合、電極間の間隔は $127\mu\text{m}$ しかなく、それに対して、ハンダのはみ出し量は最大で $80\mu\text{m}$ 程度、両側電極で $160\mu\text{m}$ 程度まで生じることがあり、そのために、隣接電極同士が接触してしまうことがある。

【0085】一方、接続の為の半田の量が少ない（半田層の厚さが薄い）と、十分な接続が行われず、接触不良が生じ易くなる。また、半田の量が多すぎると（半田層の厚さが厚い）と、熱圧着時の加圧によって半田が電極部から大きくはみ出してしまうことになる。したがって、半田の厚さには最適値があるが、信頼性良く接続しようと場合には、上述したように、ハンダのはみ出し量は、最大 $80\mu\text{m}$ 程度、両側電極で $160\mu\text{m}$ 程度まで生じて、隣接電極同士が接触してしまうことが生じる。

【0086】そこで、本実施形態においては、裏面個別電極パターン33は、スルーホール1つおきに取出し方向を異ならせている。したがって、接触領域33a同士は十分距離を確保することが可能となる。これにより、ハンダのはみ出しがあっても、隣接電極と接触する事がなく、信頼性のよいFPC実装が可能になる。

【0087】この場合、図18に示すように接触領域33a、35a以外の部分を絶縁性のレジスト69で被覆することによって、ハンダのはみ出し量以下のスペースしかないような高密度（300dpi以上）の場合でも、電極同士の接触が生じることがなくなる。

【0088】次に、本発明の第6実施形態について図19を参照して説明する。プリンタ等のインクジェット記録装置（画像形成装置を含む）の高速化、あるいはカラ一化を行なった場合、例えば黒インクの複数のヘッドで印字したり、イエロー（Y）、マゼンタ（M）、シアン（C）、ブラック（K）の4色、あるいは薄いマゼンタ、シアンを加えた6色、レッド（R）、グリーン（G）、ブルー（B）を加えた7色といったマルチヘッドで印写を行なうことになる。

【0089】本実施形態においては、2つのヘッド81を1枚のFPC82に実装している。各ヘッド81は、前述したようにスルーホールが形成され、裏面においてFPC82と接続する構成である。このように裏面でF

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P Cと接続することにより、FPC接続が容易になり、また、ヘッドの幅が必要最低限に小さくて良いので、マルチヘッドの場合の小型化を実現できる。もちろん、2つのヘッドだけでなく、さらに3個以上のヘッドを同一FPC上に形成することもできる。

【0090】なお、上記各実施形態においては、圧電素子をアクチュエータ手段に用いるピエゾ型インクジェットヘッドに本発明を適用した例で説明しているが、発熱抵抗体を用いるバブル型インクジェットヘッドにも適用することもでき、また振動板とこれに対向する電極との間の静電力を利用する静電型インクジェットヘッドにも適用することができる。

【0091】

【発明の効果】以上説明したように、請求項1のインクジェット記録装置によれば、インクジェットヘッドの圧力発生手段を設けた基板には圧力発生手段を設けた面以外の面と圧力発生手段とを接続する接続手段を設け、更にこの接続手段を形成した領域以外の領域でプリント基板と接続する接続パターンを設けた構成としたので、信頼性が向上し、引出電極部分が短くなつて小型化、低コスト化を図れる。

【0092】請求項2のインクジェット記録装置によれば、上記請求項1のインクジェット記録装置において、接続手段は基板に形成した貫通孔を介して圧力発生手段を設けた面以外の面と圧力発生手段とを接続し、基板の裏面に接続パターンを設けた構成としたので、信頼性が向上し、引出電極部分が短くなつて小型化、低コスト化を図れる。

【0093】請求項3のインクジェット記録装置によれば、上記請求項1又は2のインクジェット記録装置において、プリント基板のパターンを接続する領域を除く領域の少なくとも一部を絶縁性を有する材料で被覆した構成としたので、プリント基板実装時の電極間ショートを防止できて信頼性が向上するとともに、歩留まりが向上し低コスト化を図れる。

【0094】請求項4のインクジェット記録装置によれば、上記請求項1乃至3のいずれかのインクジェット記録装置において、接続パターンの最大配列ピッチが接続手段の配列ピッチ以上である構成としたので、プリント基板実装時の電極間ショートを防止できて信頼性が向上するとともに、小型化を図れる。

【0095】請求項5のインクジェット記録装置によれば、上記請求項1乃至4のいずれかのインクジェット記録装置において、接続手段が複数列配置されている構成としたので、信頼性ある実装を行うことができて、高密度化を図れる。

【0096】請求項6のインクジェット記録装置によれば、上記請求項1乃至5のいずれかのインクジェット記録装置において、接続パターンのプリント基板の接続部が複数列配置されている構成としたので、信頼性ある実

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装を行うことができて、高密度化を図れる。

【0097】請求項7のインクジェット記録装置によれば、上記請求項1のインクジェット記録装置において、圧力発生手段を2列以上配置し、それぞれに対応する2列以上の接続手段を設け、プリント基板との接続部を接続手段の内側に設けた構成としたので、ヘッドの小型化を図れる。

【0098】請求項8のインクジェット記録装置によれば、上記請求項1乃至7のいずれかのインクジェット記録装置において、接続パターンのプリント基板との接続部が接続手段の両側に配置されている構成としたので、信頼性ある実装を行うことができて、高密度化を図れる。

【0099】請求項9のインクジェット記録装置によれば、上記請求項1乃至8のいずれかのインクジェット記録装置において、接続パターンとプリント基板とを異方導電材料で接続した構成としたので、高密度化を図れる。

【0100】請求項10のインクジェット記録装置によれば、上記請求項1乃至9のいずれかのインクジェット記録装置において、複数のインクジェットヘッドを搭載し、そのうちの少なくとも2以上のインクジェットヘッドが1つのプリント基板上に設けられている構成としたので、マルチヘッドの小型化を図れる。

【図面の簡単な説明】

【図1】本発明の第1実施形態に係るインクジェット記録装置のインクジェットヘッド部の一例を示す外観斜視図

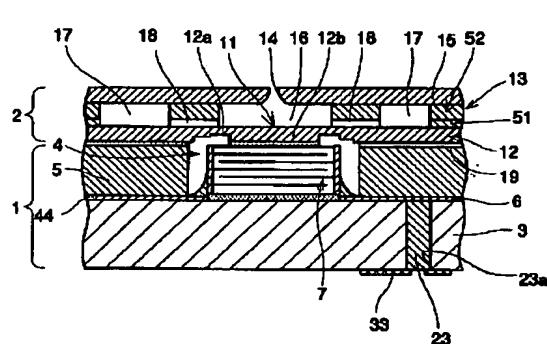
【図2】同インクジェットヘッドの分解斜視図

【図3】図1のA-A線に沿う要部拡大断面図

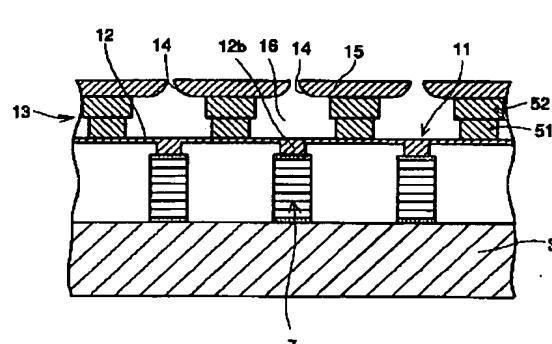
【図4】図1のB-B線に沿う要部拡大断面図

【図5】図3の要部拡大図

【図6】同ヘッドの基板の裏面説明図



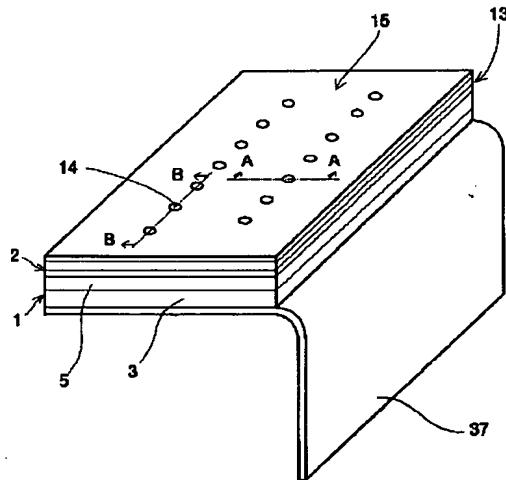
【図3】



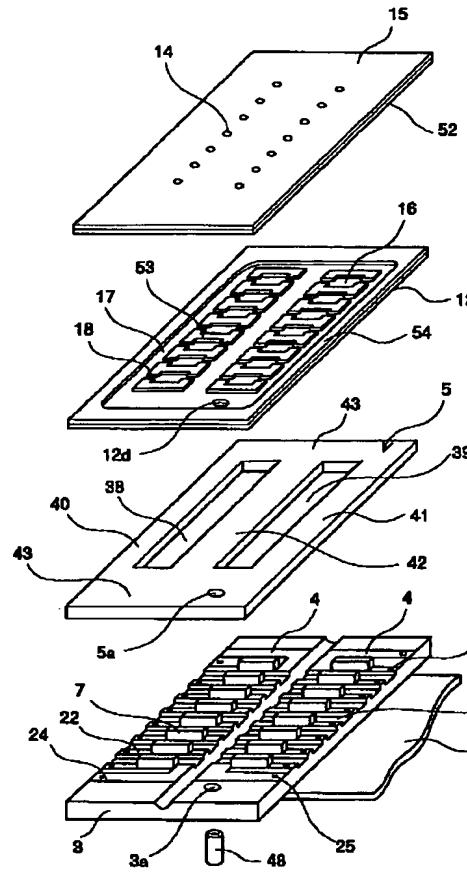
【図4】

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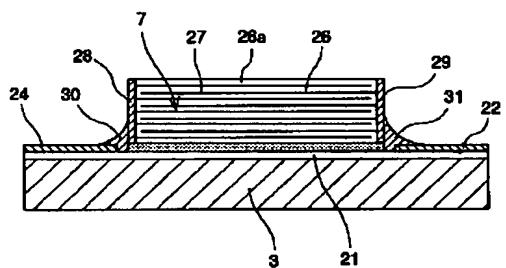
【図1】



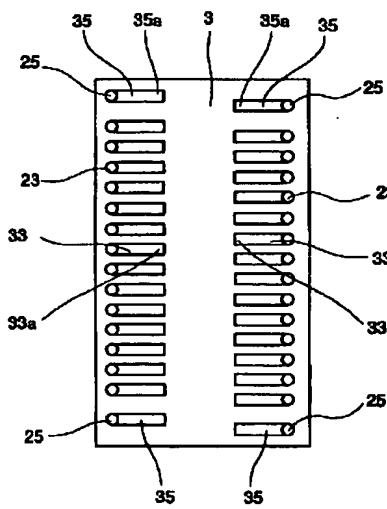
【図2】



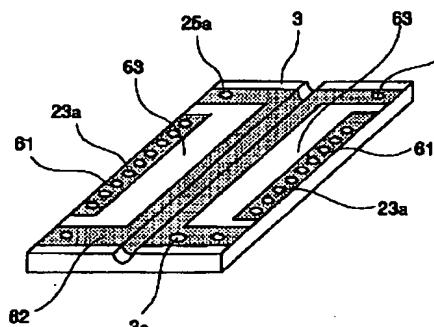
【図5】



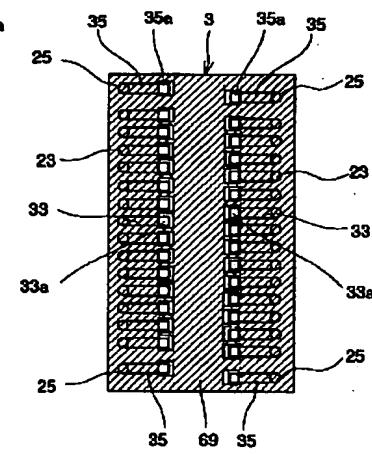
【図6】



【図7】



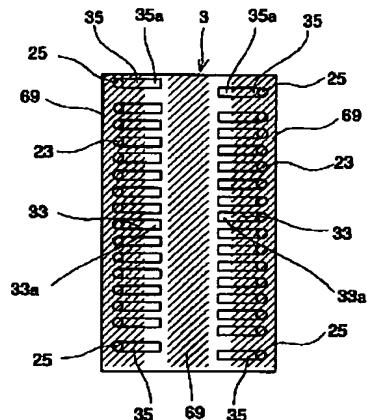
【図8】



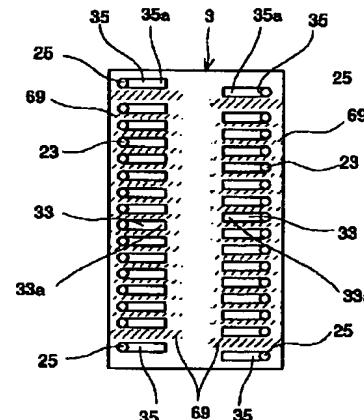
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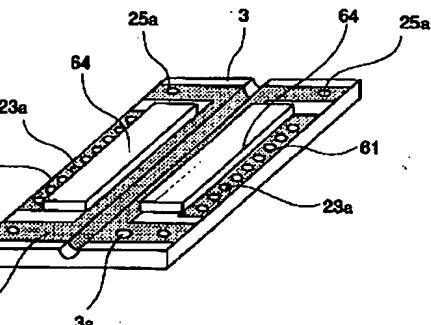
【図9】



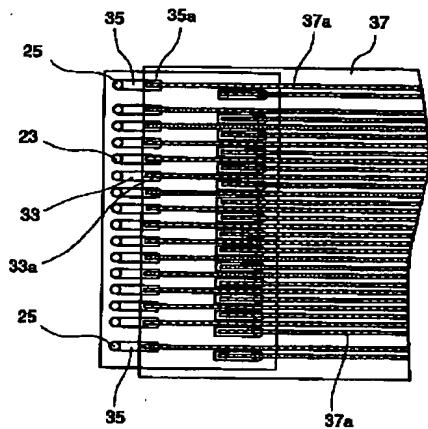
【図10】



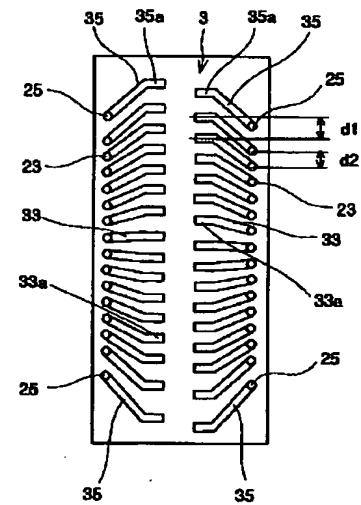
【図11】



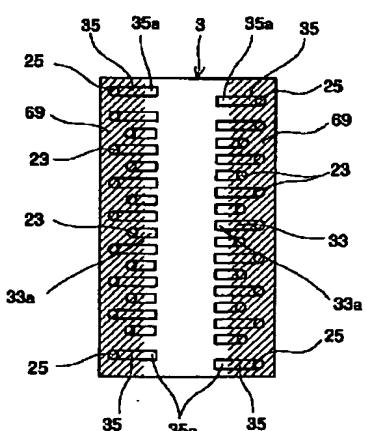
【図12】



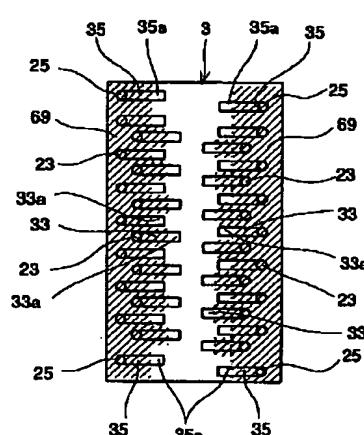
【図13】



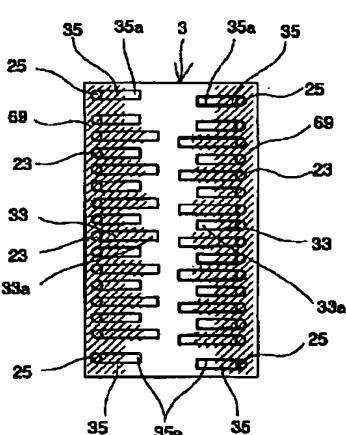
【図14】



【図15】



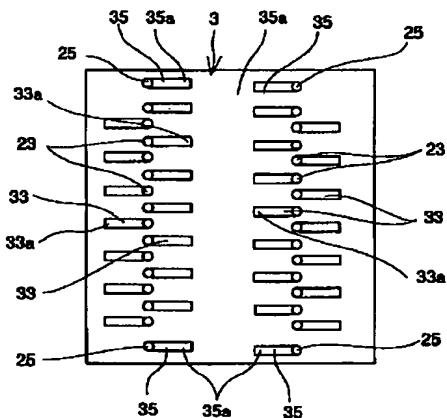
【図16】



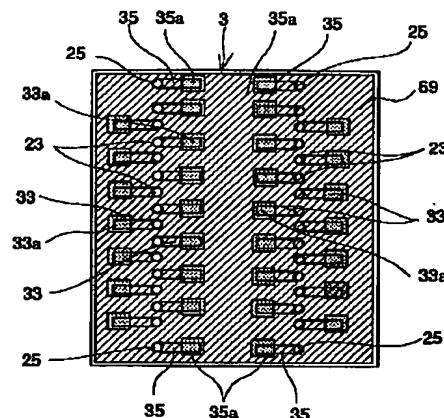
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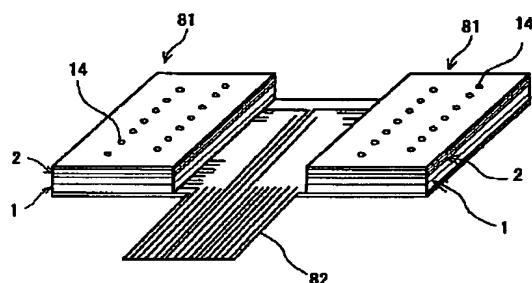
【図17】



【図18】



【図19】



フロントページの続き

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AP22 AP25 AP47 BA04 BA14